DEPARTMENT OF TRANSPORTATION COAST GUARD

BULLETIN NO. 65

Report of the International Ice Patrol Service in the North Atlantic Ocean

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Detachment operated from St. John's, Newfoundland averaging a patrol every other day over the Grand Banks. The season officially closed on 22 July 1979.

During the 1979 season, an estimated 152 icebergs drifted south of 49 degrees North.

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MAILING ADDRESS: G-OMI/31 U.S. Coast Guard Washington, D.C. 20593 (202) 426-1881

Bulletin No. 65

REPORT OF THE INTERNATIONAL ICE PATROL SERVICES IN THE NORTH ATLANTIC OCEAN,

Season of 1979.

© CG-188-34

FOREWORD

Forwarded herewith is Bulletin No. 65 of the International Ice Patrol describing the Patrol's services, and ice observations and conditions during the 1979 season.

B. F. HOLLINGSWONTH
Acting Chief, Office of Operations is tribution/

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PREFACE

This is the 65th in a series of annual reports on the International Ice Patrol Service in the North Atlantic. It contains information on ice conditions and Ice Patrol operations for 1979.

The Marine Science Branch, Coast Guard Atlantic Area, prepares this report and acknowledges the assistance and information provided by the Canadian Department of the Environment, U.S. National Weather Service, U.S. Naval Weather Service, U.S. Coast Guard Oceanographic Unit and the U.S. Coast Guard Research and Development Center. We thank Lewis Research Center, National Aeronautical and Space Administration for their continuing effort to improve RADAR detection of icebergs.

We extend our sincere appreciation to the staff of Canadian Coast Guard Radio Station St. John's/VON for their excellent support during the 1979 Ice Patrol Season.

INTERNATIONAL ICE PATROL, 1979

The U.S. Coast Guard conducted the 1979 International Ice Patrol Service in the North Atlantic Ocean under the provisions of Title 46, U.S. Code, Sections 738, 738a through 738d, and the International Convention for the Safety of Life at Sea (SOLAS), 1960, regulations 5–8. During the 1979 season, the International Ice Patrol disseminated information to the mariner on the ice conditions in the Grand Banks region of the Northwest Atlantic. To achieve this, the U.S. Coast Guard patrolled the southeastern, southern and southwestern limits of icebergs and maintained a plot on the extent of this dangerous region.

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Preseason reconnaissance flights in January and February 1979 determined the early season iceberg distributions. Based on these flights the season commenced 6 March 1979. From that date until 21 July 1979, an Aerial Ice Reconnaissance Detachment operated from St. John's, Newfoundland averaging a patrol every other day over the Grand Banks. The season officially closed on 22 July 1979.

During the 1979 season, an estimated 152 icebergs drifted south of 48°N. Table 1 shows monthly estimates of bergs that crossed 48°N.

Table 1—ESTIMATED NUMBER OF ICEBERGS SOUTH OF LATITUDE 48N, SEASON 1979

	SEP	OCT	NOV	DEC	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	TOTAL
1979	0	0	0	0	0	5	20	81	34	9	3	0	152
TOTAL 1946–1979	10	2	4	11	64	269	1100	3060	2966	1767	486	100	9839
AVERAGE 1946-1979	0	0	0	0	2	8	32	90	87	52	14	3	285
TOTAL 1900-1979	256	109	110	91	184	721	3202	7905	10,049	5285	1682	489	30,083
AVERAGE 1900-1979	3	1	1	1	2	9	40	99	126	66	21	6	377

AERIAL ICE RECONNAISSANCE

During the 1979 Ice Patrol Season (considered from 1 September 1978 through 31 August 1979) there were 145 aircraft sorties flown in support of International Ice Patrol. These included preseason surveys, ice observation flights and logistic flights. Preseason flights determine iceberg concentrations north of 48°N which are necessary to estimate the time when icebergs will threaten the North Atlantic Shipping Lanes in the vicinity of the Grand Banks. During the active season, ice observation flights map the southwestern, southern and southeastern limits of icebergs. Logistics flights were necessary to rotate ice reconnaissance detachment personnel and for aircraft maintenance. Table 2 shows aircraft utilization during the 1979 season.

U.S. Coast Guard C-130 aircraft, deployed from either Coast Guard Air Station Elizabeth City, North Carolina or Clearwater, Florida, conducted the Aerial Ice Reconnaissance. These aircraft operated from St. John's, Newfoundland.

Table 2—Aerial ice Reconnaissance 1 September 1978 to 31 August 1979

Ice Recon Flights	Number of flights	Number of hours
Preseason/		
Postseason	16	66.8
In Season	116	472.2
Logistics	13	39.9
Totals	145	578.9

NOTE In season flights include transport of personnel to and from St. John's for normal crew rotation. There were 73 sorties dedicated to ice reconnaissance.

Ice Recon Flights	Month	Flights
	FEB	2
	MAR	16
	APR	13
	MAY	18
	JUN	16
	JUL	9
Totals	_	73

COMMUNICATIONS

U.S. Coast Guard Communications Station NMF/NIK Boston, MA was the primary radio station used for the dissemination of the daily ice bulletin and facsimile chart. The Ice Patrol Office in New York prepared the bulletin and chart and sent it to numerous radio stations which broadcast the bulletin to mariners.

As in the past, the Ice Patrol Office requested all ships to report ice sightings, weather and sea surface temperatures to U.S. Coast Guard Communications Stations. Response to this request was good as shown in Table 3. The 10 most frequent contributors of this information were:

M/V BAKKAFOS/TFXO USCGC EVERGREEN/NRXD M/V KANSAS GETTY/DSOP M/V GEM/5LSU
M/V KARA/OIVD
M/V SUSANNE/5DNU
M/V ATLANTIC PREMIER/SFHN
M/V STOVE TRADER/LDGS
M/V VISEU/YODH
M/V WEYROL/HPWO
Appendix A lists all contributors.

Table 3

Number of ships furnishing SST reports	71
Number of SST reports received	397
Number of ships furnishing ice reports	76
Number of aircraft furnishing ice reports	3
Number of ice reports received	183
First Ice Bulletin 060000Z M	1AR79
Last Ice Bulletin 220000Z.	JUL79

ICE & ENVIRONMENTAL CONDITIONS

September-December 1978

Figures 1 through 3 illustrate the growth of sea ice during this period. By December ice was as far south as the Strait of Belle Isle and extended 100 miles or more off the Labrador Coast. Iceberg sightings during this period were infrequent with Ice Central Ottawa reporting some icebergs in the waters off the Labrador Coast. Figures 20 through 23 depict surface pressure characteristics that contributed to ice formation and movement. During this period conditions were near normal, with predominately westerly winds and no unusual ice conditions noted.

January-February 1979

Ice formation continued as shown in figures 4 and 5. By mid-February sea ice extended south as far as Cape Bonavista and out to 50 miles off the coast of Newfoundland. In early February the Ice Patrol conducted the first aerial reconnaissance of the 1979 season. Icebergs were sighted off the Coast of Labrador and by late February icebergs were probably crossing 48°N though there were no reconnaissance flights to verify this until early March. The average surface pressures shown in figures 24 and 25 indicate that a strong northerly flow existed in February creating the ideal conditions for moving ice and icebergs south towards the shipping lanes.

March 1979

Limited reconnaissance during January and February led to the Ice Patrol conducting a comprehensive survey of the waters off Newfoundland during the first week of March. Icebergs were observed south of 48°N and as a result the Ice Patrol commenced broadcast of ice conditions on 6 March 1979. Figure 13 shows the estimated ice conditions at that time. Sea ice reached its southern limit during this month as seen from figure 6. However, the approaches to the Strait of Belle Isle and St. John's were covered by as much as seven oktas of sea ice. The ice conditions for 24 March are shown in figure 14. The average surface pressures for March (figure 26)

resulted in predominantly westerly air flow which kept the bergs offshore and ensured their clear passage southward. The estimated number of icebergs crossing 48°N for March was 20.

April 1979

April marked the beginning of the sea ice retreat and was also the heaviest single month for icebergs crossing 48°N. An estimated 81 bergs drifted south during this month. Some typical ice conditions are shown in figures 7 and 15. It was during April that significant changes in weather patterns occurred that led to prevailing onshore breezes and the drift of icebergs out of the Labrador Current and towards the coast. This resulted in fewer bergs reaching the Grand Banks and a reduced hazard to shipping. Figure 27 shows the average surface pressures and the low pressure system east of Newfoundland that dominated the weather for April.

May 1979

The unusual weather patterns of April continued to dominate through May. The weak low pressure system was moved east by a ridge of high pressure as seen in Figure 28. The result was a still persistent onshore breeze and a corresponding shoreward drift of ice and icebergs. Sea ice conditions are shown in figure 8; iceberg conditions for 1 May and 31 May are shown in figures 16 and 17. These figures show the trend towards shoreward drift and reduced numbers of icebergs that developed during this month. In May an estimated 34 bergs drifted south of 48°N. However, reconnaissance flights north along the coast of Labrador sighted hundreds of icebergs that would have drifted further south if they had not been blown out of the main stream of the Labrador Current.

June 1979

By June it was apparent that the iceberg threat to shipping was greatly diminished and that few bergs would drift south towards the Grand Banks. Sea ice drifted no further south than the Labrador Coast and only an estimated nine bergs crossed 48°N. Ice conditions for 12 and 24 June are shown in figures 9 and 18. These show that most of the ice was well north of the major shipping lanes and with the increased water temperatures in that area few bergs were likely to survive the drift south and become a hazard.

The average surface pressure shown in figure 29 indicate a return to near normal conditions. The onshore breeze was no longer a predominant force but, as mentioned, the higher water temperatures took over where the breeze left off in preventing southward drift.

July-August 1979

July was the last month that Ice Patrol conducted reconnaissance operations; the last

flight was made on 19 July with no icebergs sighted in the vicinity of the Grand Banks. An estimated 3 icebergs drifted south of 48°N during July. Sea ice and iceberg conditions for late July are shown in figures 10 and 19. Sea surface pressures are shown in figures 30 and 31. Sea ice conditions for August are in figure 11; the retreat continued as seen in figure 12.

Iceberg reports continued to arrive through August but no bergs were noted south of the approaches to the Strait of Belle Isle. As is quite common, icebergs remained in that area and Ice Patrol forwarded all berg reports to Ice Central Ottawa which broadcast the information to North Atlantic mariners.

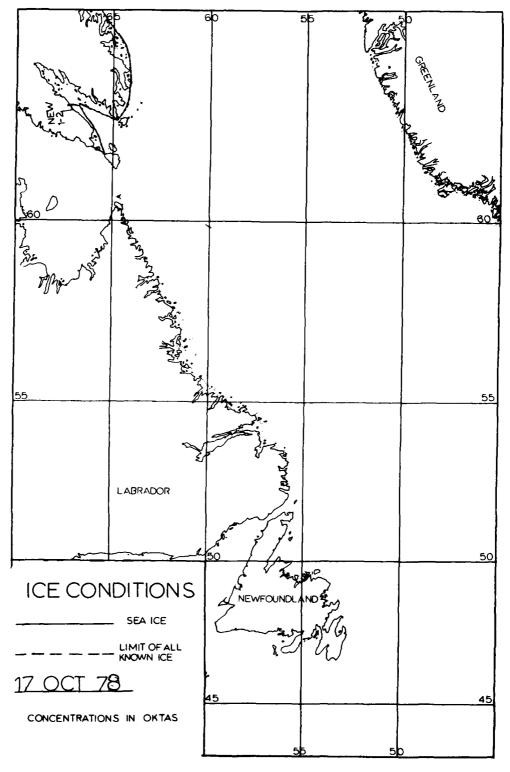


Figure 1

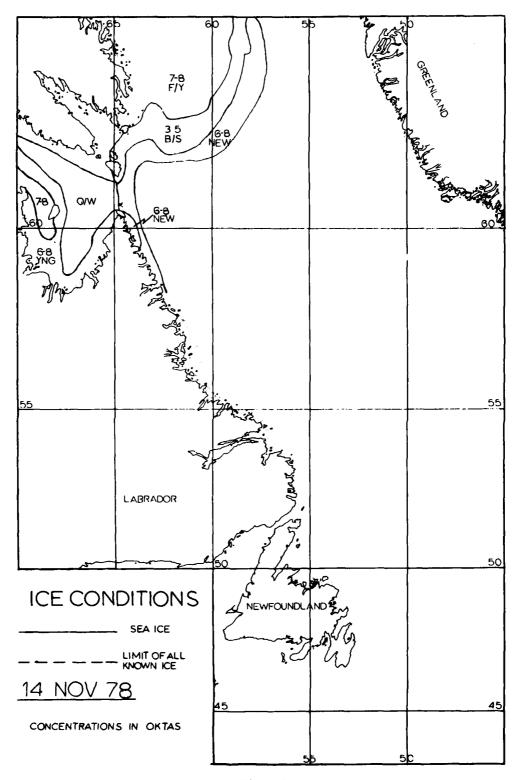


Figure 2

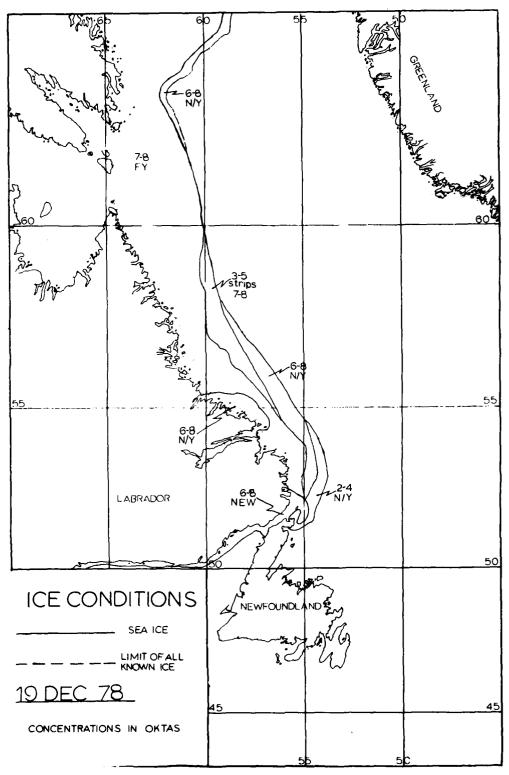


Figure 3

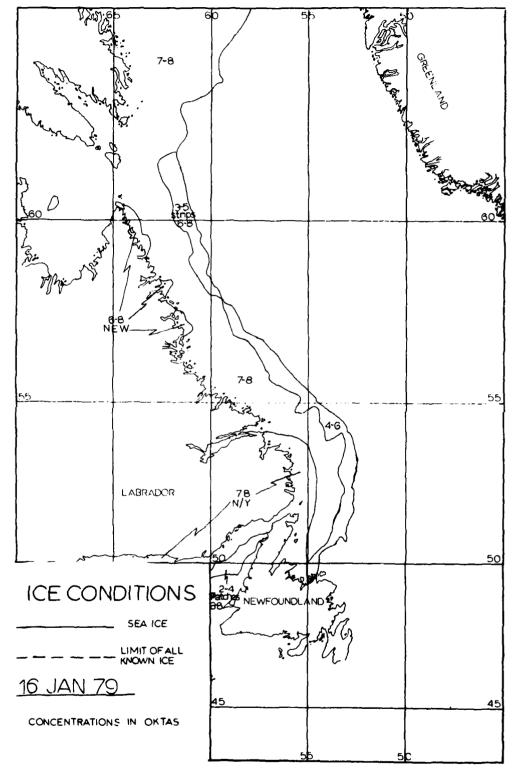


Figure 4

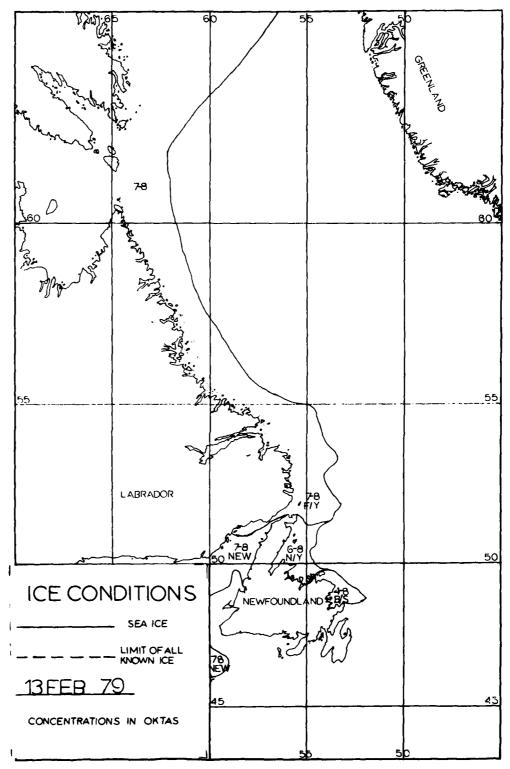


Figure 5

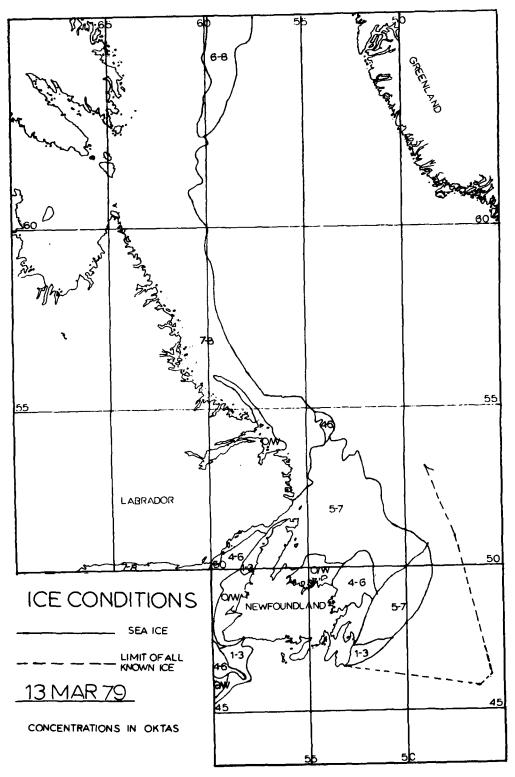


Figure 6

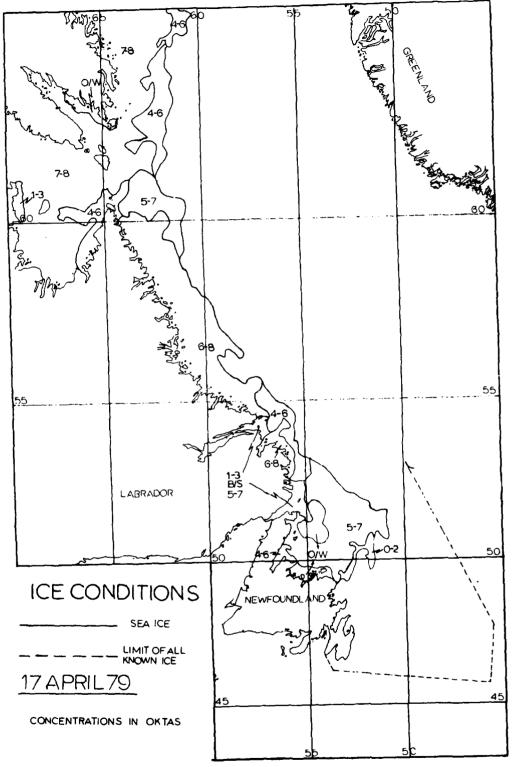


Figure 7

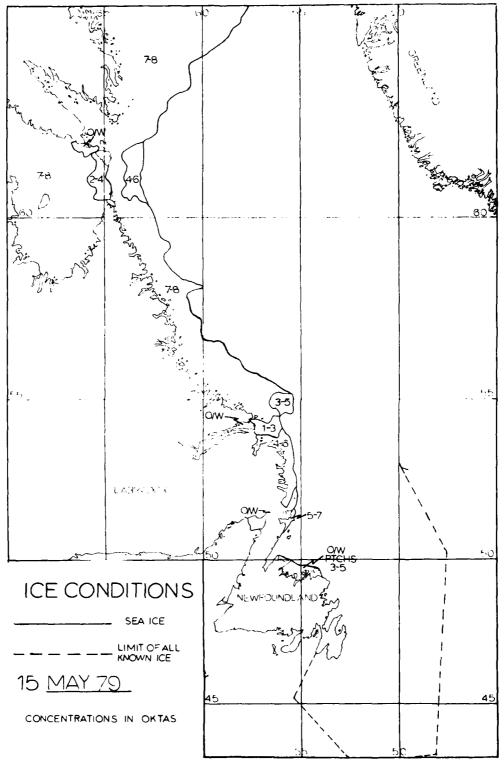


Figure 8

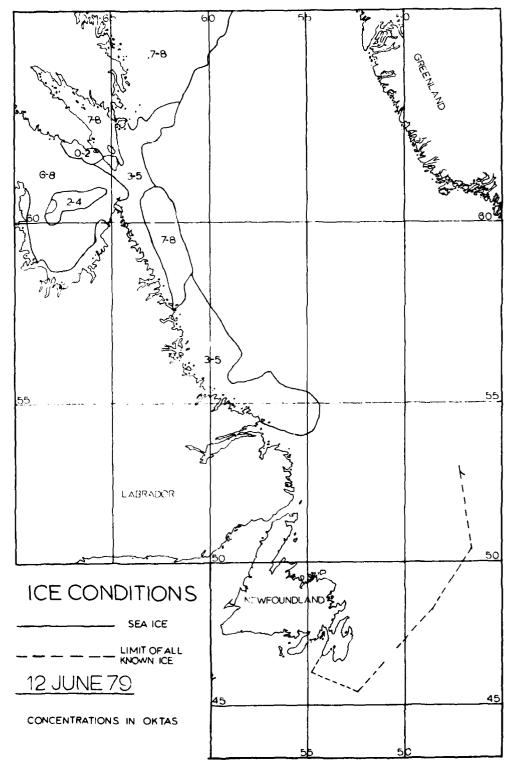


Figure 9

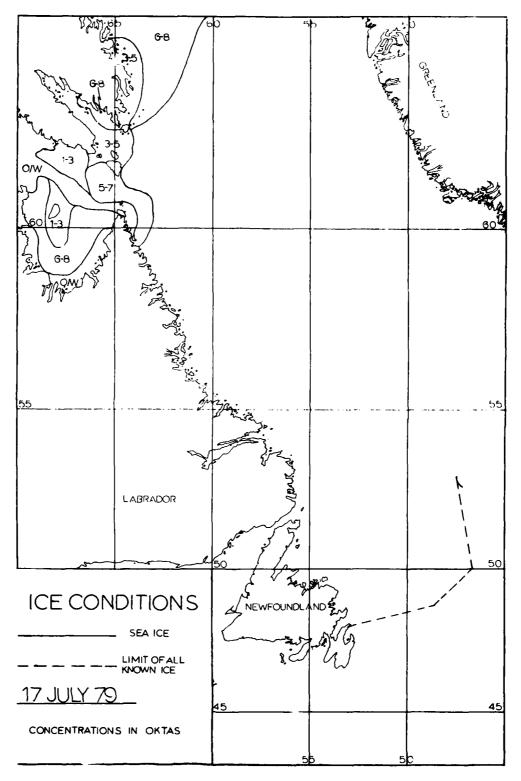


Figure 10

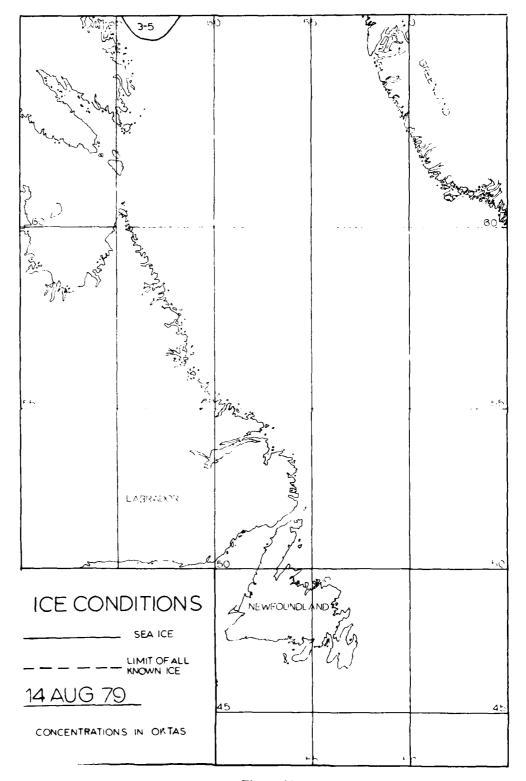


Figure 11

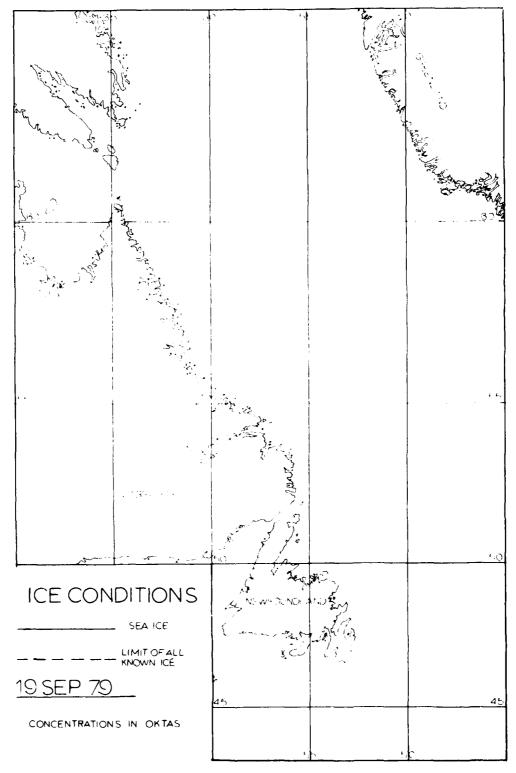


Figure 12

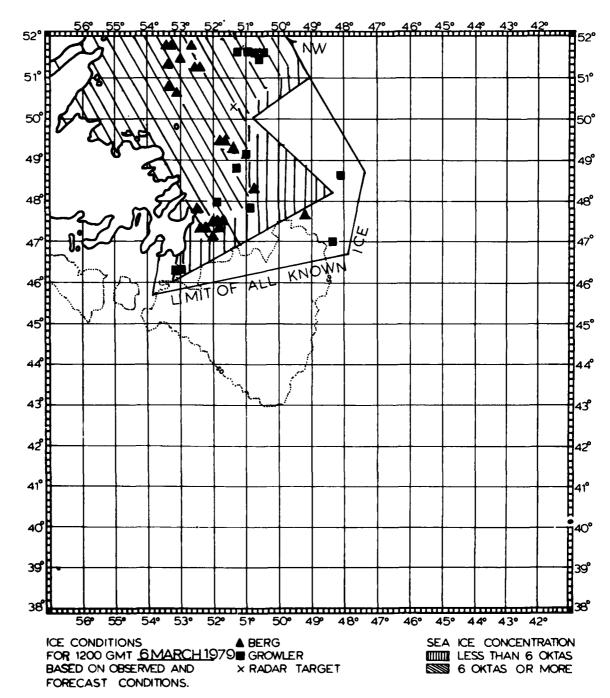


Figure 13

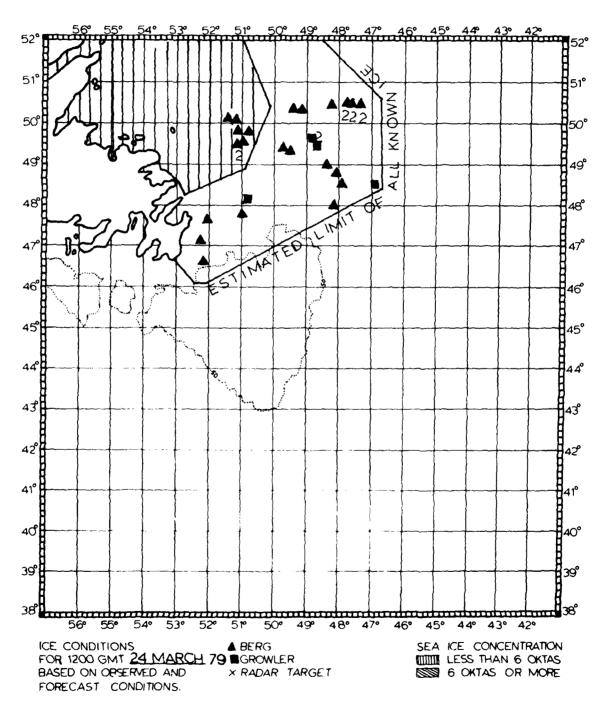


Figure 14

لإيلا المان المحميد المستدارينيوروسيد

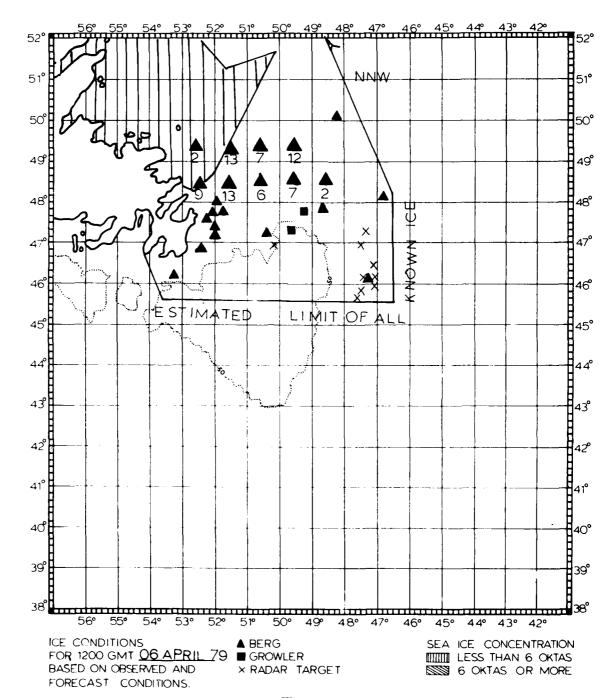


Figure 15

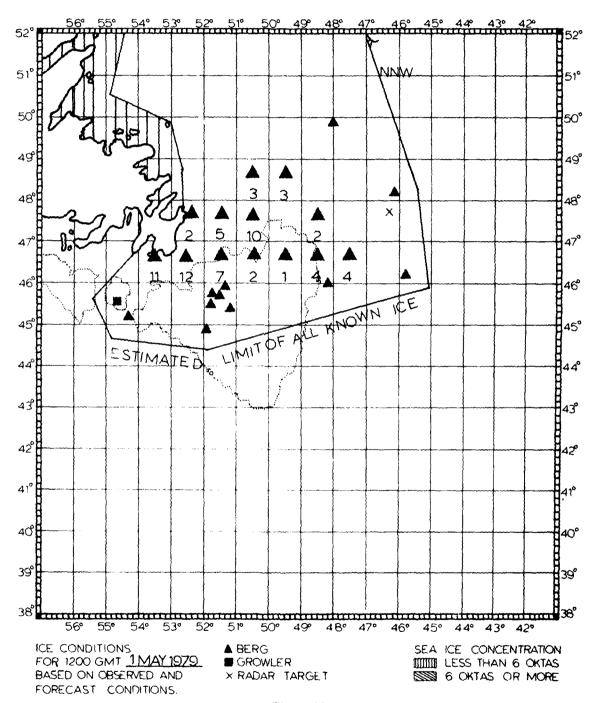


Figure 16

يهايها الطوار ويلامهم والأراز والمدارسي ماما

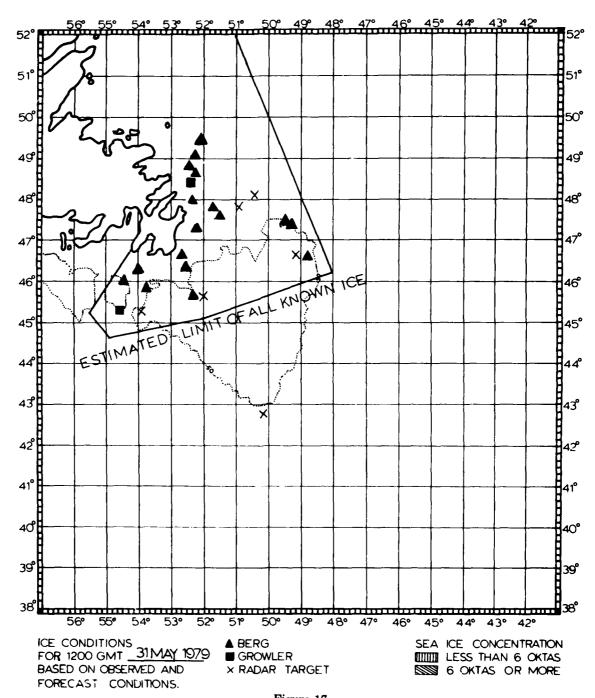


Figure 17

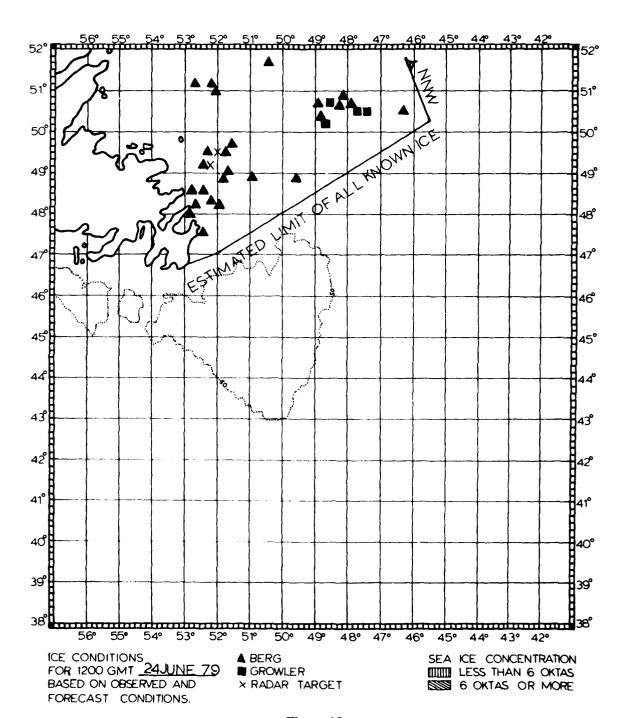


Figure 18

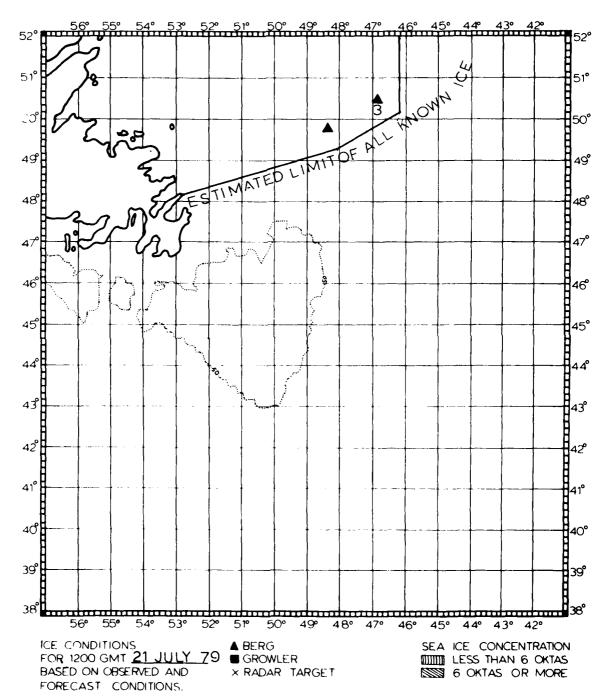


Figure 19

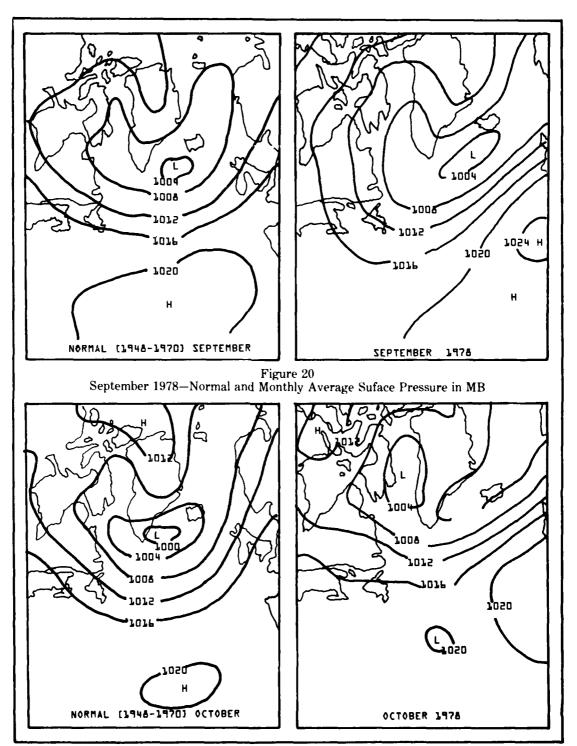


Figure 21
October 1978-Normal and Monthly Average Suface Pressure in MB

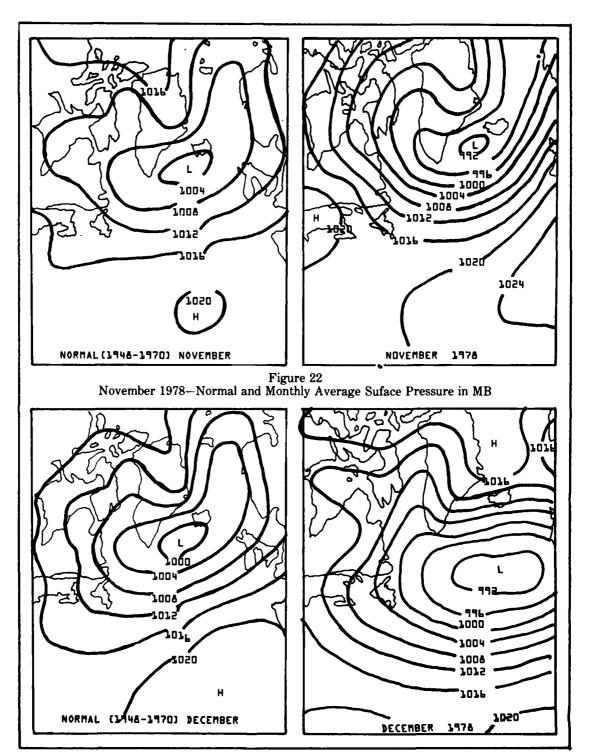


Figure 23
December 1978—Normal and Monthly Average Suface Pressure in MB

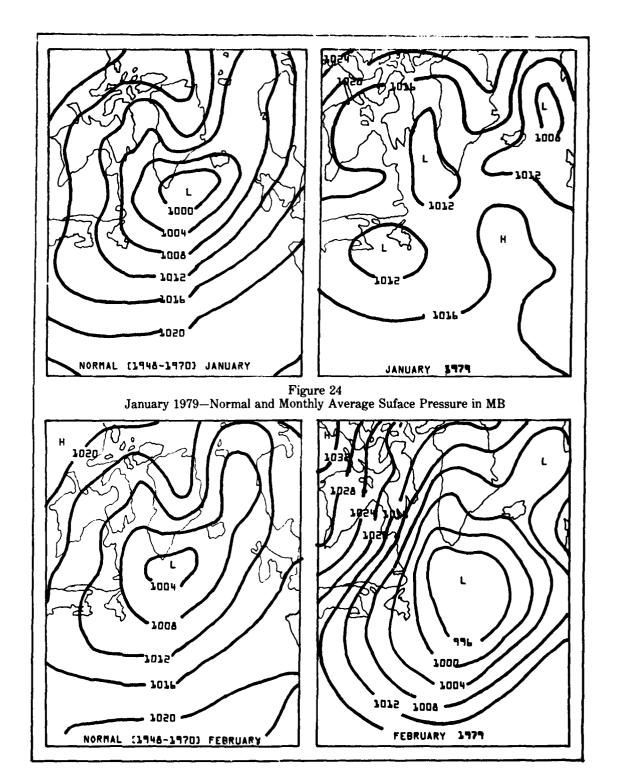


Figure 25
February 1979—Normal and Monthly Average Suface Pressure in MB

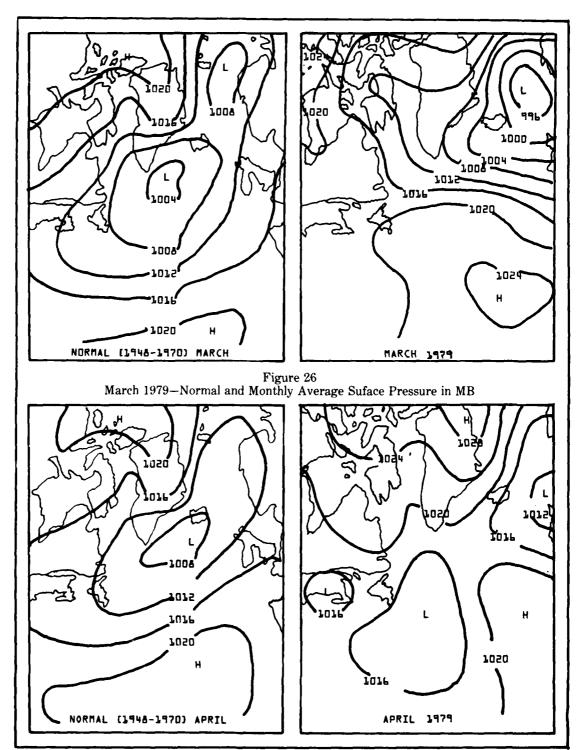


Figure 27
April 1979-Normal and Monthly Average Suface Pressure in MB

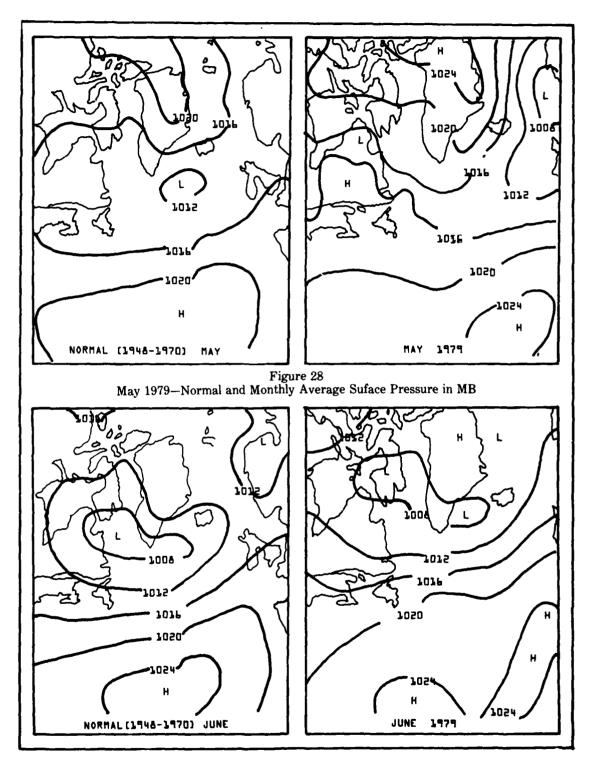


Figure 29
June 1979—Normal and Monthly Average Suface Pressure in MB

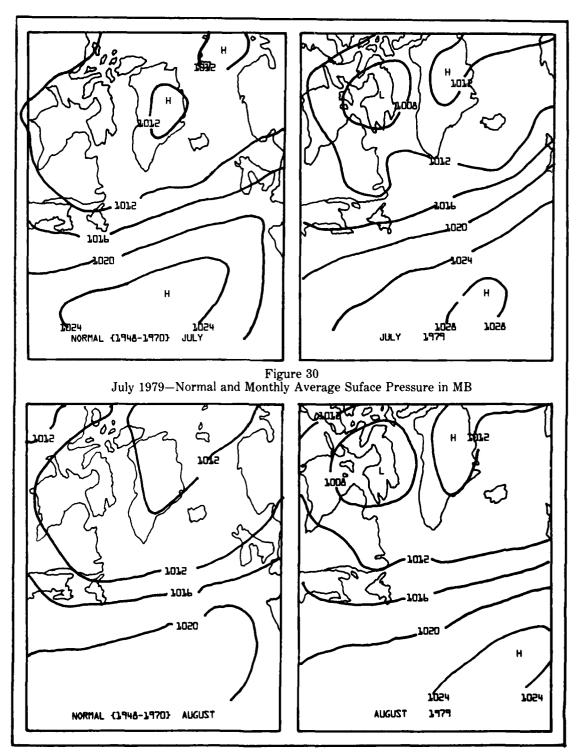


Figure 31
August 1979—Normal and Monthly Average Suface Pressure in MB

APPENDIX A CONTRIBUTING VESSELS

SHIP'S NAME	COUNTRY OF REGISTRY	ICE REPORTS	SST REPORTS
Nememcha	Algeria		3
Petimata	Bulgaria	1	
Algonquin	Canada	2	4
Bartlett	Canada	1	
Breton Shore	Canada	1	
Federal Avalon	Canada	2	
Hudson	Canada	3	
Imperial Arcadia	Canada	1	
Janie B	Canada	1	
Kathy C	Canada	1	
Mare Placido	Canada		1
NFLD Cont	Canada	3	
Nonia	Canada	3	
Hadan	Cyprus	1	
Belgium	Czechoslovakia	1	
Artic Skou	Denmark	3	
Kara	Finland	1	19
Peter	Finland		5
Atlantic Cognac	France	1	
Denmarch	France	2	
Anne Marie Krueger	Germany	2	2
Balder Alver	Germany		2
Danis Getty	Germany		1
Fjellnes	Germany	1	
Koeln Express	Germany	3	
Dynamic Sailor	Greece	1	5
Evpo Sailor	Greece	2	
Irenes Ideal	Greece	_	1
Konkar Indomitable	Greece	1	2
Meltemi 2	Greece	_	4
Zannis Machlos	Greece		2
Tenadores	Honduras		3
Bakkafoss	Iceland	18	52
Joekulfell	Iceland	i	
Selfoss	Iceland	_	5
Skaftafell	Iceland	1	-
Studiafoss	Iceland	2	
Jayagayatri	India	2	4
Jhanskirani	India		1
Loknanya	India		1
Samratashok	India		6
Donn arasilor	IIIUIG		U

SHIP'S NAME	COUNTRY OF REGISTRY	ICE REPORTS	SST REPORTS
Jordan Kanikolova	Indonesia		2
Mezada	Israel	2	
Adria Maru	Japan		6
Miho Maru	Japan		1
Teruoku Maru	Japan		10
Amax Miner	Liberia	2	
Artadi	Liberia	4	4
Corner Brook	Liberia		3
Eastern Hazel	Liberia		5
Federal Hudson	Liberia	1	
Garden Gate	Liberia		3
Gem	Liberia	3	22
Gemini Pioneer	Liberia	2	
Kansas Getty	Liberia		2 5
Kathleen	Liberia		7
Liberian Albertwill	Liberia		2
Lupus	Liberia		1
Magic Sun	Liberia	1	
Navios Courier	Liberia		8
Pilot Trader	Liberia	1	
Ploto	Liberia		5
Ralu	Liberia		3
Santal	Liberia	1	
Torrent	Liberia		9
Weser	Liberia		6
World News	Liberia		1
Dryso	Norway	1	1
Jacara	Norway		2
Norwegian Laurita	Norway	1	1
Norwegian Tamesis	Norway	3	3
Stove Trader	Norway	4	11
Charlotte Bastian	Panama	3	4
Discoverer Seven Seas	Panama	_	6
Margitta	Panama	1	
Weyroc	Panama	_	11
Ammbrow	Poland	1	
Stefan Batory	Poland	10	
Zambrze	Poland	1	
Ziemia Olsztynska	Poland	1	
Viseu	Romania	6	6
Hinrich Oldendorff	Singapore		1
Macarena	Singapore	1	3
Marques DeBolarque	Spain	1	•
Atlantic Premier	Sweden	i3	3
Atlantic Saga	Sweden	3	3
Atlantic Wasa	Sweden	4	5
Ivan Gorthan	Sweden	1	
Marine Atlantica	Sweden	1	
Stolt Castle	Sweden	1	4.5
Susanne	Sweden		17
Romandie	Switzerland		5

SHIPS NAME	COUNTRY OF REGISTRY	ICE REPORTS	SST REPORTS
Silveretta	Switzerland		1
Asian Reward	United Kingdom		1
Athel Monarch	United Kingdom		1
Atlantic Prosper	United Kingdom	1	1
British Wasa	United Kingdom		4
Cast Seal	United Kingdom	1	
C.P. Discoverer	United Kingdom	1	
C.P. Trader	United Kingdom	4	
C.P. Voyager	United Kingdom	2	
Fort Hamilton	United Kingdom	5	
Kayeson	United Kingdom		3
Kildare	United Kingdom		6
La Costa	United Kingdom		4
La Ensenada	United Kingdom		6
Manchester Concept	United Kingdom	2	
Manchester Concorde	United Kingdom	3	2
Manchester Renown	United Kingdom	6	
Reynoulds	United Kingdom	1	
Roebuck	United Kingdom	1	1
Rubens	United Kingdom	1	
Salters Gate	United Kingdom	1	4
Tsuru Arrow	United Kingdom	1	6
W.M. Neal	United Kingdom	1	
Detroyat	USSR		1
Martha Progress	USSR		2
Evergreen (USCGC)	USA	7	26
Pioneer Crusader	USA	1	
Sealift Indian Ocean (USNS)	USA	1	
Sealand Galloway	USA	1	
Westwind (USCGC)	USA	3	
	TOTAL	180	397

APPENDIX B

OCEANOGRAPHIC CONDITIONS

LT J. J. MURRAY, U.S. Coast Guard

BACKGROUND

The 1979 season witnessed significant changes to the Ice Patrol mode of operation. In February 1979 a new computer model to predict the drift of icebergs was accepted as operational by Commander, International Ice Patrol (CIIP) and was used throughout the season. The IIP current file used in this model was also updated to include information obtained since its establishment in 1964. Perhaps most significantly, traditional standard oceanographic surveys were replaced with satellite tracked buoys as the primary method of measuring currents and verifying the IIP current file.

A NEW ICEBERG DRIFT PREDICTION MODEL

During the 1979 ice season a new computer model was used to predict the drift of icebergs. The drift model, termed IBERG, was developed at the Coast Guard Oceanographic Unit during the fall of 1977, and was tested during the 1978 ice season. The model was then integrated into the operational Ice Patrol system and accepted for operational use in February 1979.

IBERG forecasts the drift of an iceberg by solving differential equations of motion that express the forces acting on the iceberg. The forces included are the Coriolis force, the wind drag, the water drag, and a gravitational component due to the slope of the sea surface. The equations are solved by a fourth order Runge-Kutta method using a variable time step to insure a convergent solution.

The primary improvement over past modeling efforts is in the calculation of the water drag, which is usually the dominant forcing term. The water drag is proportional to the iceberg cross-sectional area and the square of the velocity of the ice relative to the water. The water current used is the sum of a mean value and a wind driven component that is derived from a solution to a time

dependent Ekman equation using a 96 hour wind history. The average Ekman current in each of four layers of the water column is determined. The water drag in each layer is calculated and the results are summed to yield the total drag over the iceberg. This approach allows different sizes of icebergs to be modeled by varying the cross-sectional area in each layer. Small icebergs float in the near surface layer which is strongly affected by the local wind, while large icebergs have much of their area below the wind-influenced layers. Seven iceberg sizes are allowed in the operational form of IBERG.

A continuing evaluation of IBERG is being conducted. Observed iceberg drift tracks are compared to model generated paths to estimate the model accuracy. Initial results suggest that the primary limitation to accurate forecasts lies in the inputs to the model, most notably the current and wind fields used in the drag calculations.

IIP CURRENTS

The IIP current file extends from 40°N to 52°N and from 39°W to 57°W. Within this area are two regions. The currents are best known in the first region in the proximity of the Labrador Current where standard oceanographic surveys were conducted under the auspices of CIIP every seasor. from 1934 to 1978 (except during World War II). Usually 2 or 3 surveys were made each season. These surveys yielded a large data base which was used in 1964 (Soule, 1964) to compile "normal" dynamic topography charts representing the average dynamic heights observed up to that time. From these charts normal geostrophic velocities were calculated. The normal values are useful because the general oceanic circulation in the Ice Patrol area is similar from year to year. The normals were reviewed and updated in 1976 (Scobie and Schultz, 1976) and it is basically these updated currents which were used during the 1979 season. The second region is composed of all other currents within the IIP current file. They were compiled by CIIP from various sources constituting a much lower quality data base then that used for the first region.

Contained in Appendix A is a listing of the 1979 IIP current file. The current direction in degrees true and the speed in cm/s (51 cm/s = 1 knot) are listed for every 20 minutes of latitude and longitude except in the vicinity of the Labrador Current where the longitude spacing is 10 minutes. This finer grid encompasses all of region 1 and a small part of region 2. Region 1 currents in Appendix A are indicated by asterisks (*). There was only one current file for the entire 1979 season as opposed to four files which were previously used, one each for April, May, June and July. It was felt that monthly variation of currents within a given season was not large enough to warrant more than one IIP current file.

SATELLITE TRACKED BUOYS

The Oceanographic Unit began examining the feasibility of using satellite tracked drifting buoys to measure currents as early as 1975. In 1976, 1977, and 1978 satellite tracked buoy transmitting terminals (BTT's) were deployed in the Ice Patrol area and tracked using the NIMBUS-6 satellite system. Positions obtained were analyzed to determine currents. The results of these tests were so successful that the Oceanographic Unit presented a position paper at the 1978 IIP Planning Conference stating that BTT's could replace standard oceanographic surveys as the method for gathering current information to evaluate the IIP currents. This idea was accepted by CIIP and 1979 became the first season since 1948 during which no oceanographic surveys were made by a Coast Guard vessel in support of IIP operations.

The satellite system used during the 1979 Ice Patrol season was TIROS-N. When the satellite is within sight of a BTT it records the data being transmitted on 416.65 MHz. This information is processed and encoded by the TIROS information processor and retransmitted almost instantaneously on the spacecraft beacon frequency, 136.77 MHz. The ground receiving station and the BTT must both be within line of sight of the satellite for this retransmission to be received at the ground station. In the fall of 1978 a prototype Local User Terminal (LUT) was established at the Oceanographic Unit to allow relatively independent and near real-time data reception. It is capable of receiving the transmissions of both the

NIMBUS-6 and TIROS-N satellites and processing them to obtain position and sensor data. With its present location in Washington, D.C., in the TIROS-N mode the LUT normally receives information from 2 satellite passes daily with the capability of locating BTT's anywhere within the IIP area. The maximum accuracy of the system with the incorporation of adequate reference beacons is about ± 3 km (1.6 nautical miles).

The cornerstone of the new current measuring scheme is the BTT's themselves. All BTT's used are in what is called the TIROS Oceanographic Drifter (TOD) configuration (Figure 1). This includes the basic buoy, window shade drogue, the drogue sensor, temperature sensor and battery monitor. The drogue extends from about 12 to 24 m below the sea surface and is designed to reduce buoy leeway as much as possible. The temperature sensor is accurate to within ±1.0°C and provides valuable sea surface temperature data. During the 1979 season all BTT's were air deployed from Coast Guard HC-130 aircraft (although they can be ship deployed) utilizing a special air deployment package (Figures 1 and 2). The system is designed so that the BTT on a pallet is slid out the rear cargo door of the aircraft and parachutes to the sea surface. Water-activated explosive cutters cut away the parachute, and the specially designed hardware connecting the pallet to the BTT dissolves causing the pallet to fall away and the drogue to deploy. The entire process normally takes only a few minutes.

1979 OPERATIONS

During the 1979 season 5 BTT's were deployed in support of IIP operations (Table 1). Three BTT's, 2605, 2600 and 2604, were deployed in the Labrador Current, BTT 2601 was deployed to the east of the Labrador Current and BTT 2602 was deployed northeast of Flemish Cap. All 5 BTT's functioned well throughout the season. A total downtime of 18 days (7.7% of the season) was experienced on the LUT due largely to its developmental nature. Accuracy of positions was not as good as the 3 km normally attainable because of inadequacy of reference platforms. However, comparison of BTT positions with reported deployment positions and known locations of relatively swift moving currents such as the Labrador Current indicated positions were within ±10 km. Exact errors could not be determined.

The purpose of deploying BTT's was to make current measurements to compare with the IIP current file. To do this BTT positions were first input to a computer program utilizing a cubic spline routine to smooth out the drifts. The program calculated a smooth trajectory by ensuring a mathematically continuous first derivative of the BTT displacement versus time plot, thus velocity, and a minimum second derivative, thus acceleration or potential energy. It then output a printout of 6-hourly BTT positions and velocities (Table 2) and a plot of the smooth BTT trajectory (Figures 3-7) representing an approximation of the path the BTT followed. On these plots X's represent input positions, not all of which are marked, and numbers are Julian dates.

To make valid comparisons with the IIP currents, the wind current's contribution must be removed from the BTT drifts. Another program, a modified version of IBERG, used CIIP wind files to calculate wind currents using the same Ekman equation described earlier. The actual comparison of observed drifts and IIP currents was accomplished by a third program (Table 3). It computed 6-hourly observed currents with the wind current subtracted out (BTT w/o W.C.) and then vectorially subtracted the IIP (normal) current from this value. The difference was output in individual and cumulative speed and direction and U (east-west) and V (north-south) components on a printout and plots. The results were then analyzed to determine what if any changes in the current file were warranted. Magnitudes of differences, variability of currents in the respective location, time of season and reliability of measurements were among the items taken into account. No changes to the IIP current file were made during the 1979 season.

REVIEW AND OUTLOOK

The validity of the concept of using satellite tracked BTT's to measure currents was proven during the 1979 season. Even though the system was in its fledgling stages, it worked well enough to determine if changes to the HP current file were necessary.

Programs developed to analyze the BTT drifts proved adequate. Much was learned about the capabilities and limitations of the system. Several refinements are planned for the 1980 season but the general overall operational scheme will remain the same. Perhaps most significantly, since the end of the 1979 season a second satellite in the TIROS series, NOAA-6, has been launched and is operational. It will provide additional positions and thereby even more accurate evaluation of IIP currents. Additionally, several reference beacons have been procured for use to ensure maximum accuracy is obtained. Overall, during 1979 the satellite tracked buoy system provided more accurate and much more timely current measurements at a reduced cost as compared to the old survey method. With the system still developing the prospects for the future appear even brighter.

REFERENCES

Scobie, R. W. and R. H. Schultz (1976). Oceanography of the Grand Banks Region, March 1971-December 1972.
U.S. Coast Guard Oceanographic Report No. 70, Coast Guard 373-70:47.

Soule, F. M. (1964). The Normal Topography of the Labrador Current and its Environs in the Vicinity of the Grand Banks of Newfoundland during the Iceberg Season. Woods Hole Oceanographic Institution, Ref. No. 64-36.

Table 1—BTT	DATA	٩
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Buoy ID	Date	Deplo	yment	Positions/Temperatures Supplied				
		Latitude	Longitude	Total	Per Week			
2605	01 March	49-00.6	49-57.6	87	4			
2602	05 April	49-38.0	46-42.0	68	4			
2600	12 May	48-59.4	49-54.0	52	5			
2601	04 June	47-12.0	46-18.0	35	5			
2604	04 June	47-12.0	47.06.0	34	5			

NOTE: Latitude and Longitude are in degrees-minutes.

OIM (T)	145.8	143.1	148.4	170.1	219.3	242.5	247.2	241.4	228.2	•	•		246.0	251.7	256.1	240.3		260.5	245.5		192.5		148.8	:		ċ	-	÷	244.5	÷	•				•		•	235.2		•
SEC)	•	7	ŝ	8.20	₹.	10.06	4	•	10.38	•	4	2	•	21.62	22.44	22.61	21.03	18.72	16.50	17.12	22.13	23.44	3.	0	24.72	ŗ	14.79	15.14	~	7.1	0	•	40.16	ç	c	33.10	Œ	30.96	30.22	4.6
E.	c	æ				46 51.9	η.		46 56.H		59.		47 3.8		_	7	_			26		~			4.02 74			47 16.4	47 19.1	47 24.2	30	47 37.8	4	51	56.		Ġ	48 11.3	15.	_
LONG																																								
DEG-MI	12	46 11.5	_	46 9.3	æ	46 7.9	~	æ	46 6.1			m	44 2.3	44 1.5		44 0.2			45 59.0	45 57.9	'n			4% 4X.1		44			45 39.4			35.	34.	33.	32.	31.	29.	4F 27.6	25.	
LAT																																	7				•			
(NIM-S	c .	0.0	0.0	0.0	0	0.0	Ú°G	0.0	C • C	c • c	0.0	0.0	0.0	0.0	0.0	0.0	0.0	9. 0	0 • 0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	•	•	0.0	0.0	•	0.0	•	•
TIME (HR	12	18	o	r	12	18	c	ç	12	В	c	t	12	<u>~</u>	0	æ	12	18	0	ç	12	99	0	æ	12	8.	0	9	15	Ξ.	0	•	12	æ	C	£	12	1,8	c	£
ĵ	• 40	164.	165.	165.	165.	165.	166.	144.	146.	144.	167.	167.	147.	167.	168.	160.	164.	168.	169.	169.	144.	169.	170.	179.	170.	170.	171.	171.	171.	171.	172.	172.	172.	172.	173.	173.	173.	173.	174.	174.

Table 2.—Example of BTT (02604) Position, Speed and Direction output.

			į			260	2604 BIT DRIFT	IFT			
0AY 164	TIME 1200	DIST	DIST	SPEEU 12.29	UIR 145.A	~ £	01R	U 6.91	-10.16	CUM U 6.91	CUF V -10.16
						æ	BIT W/N W	U 3			
SPEFD	SPEED DIR U	2 2 2	>	11.48	146.7	11.48 146.7	146.7	6.31	65*6=	6.31	-9.59
5.16	5.16 157.2	2.00	-4.75			٥	DIFFERENCES	ES			
				6.48	138.3	Α. 4.	6.48 138.3	4.31	-4.84	4.31	14.14
DAY 164	7 IME 1800	DIST 1.58	CIIM DIST 1.58	SPEED 13.17	018 143.1	240 CUM SPEED 25.45	2404 HTT DMIFT CHM D DIR 5 144.4 7	JFT U 7.91	v -10.53	CUM U 14.83	CUM V -20.69
						ı	HTT W/O W.C.	ن			
SPEF	NORMAL D DIR	NORMAL DRIFT Spefo Dir U	>	12,35	143.7	23.83 290.4	4.042	7.30	96.6-	13.61	-19.55
6 • 3.	4.33 142.4	5.64	-3.44			C	DIFFERENCES	ri S			
				A.02	144.4	14.49	282.8	4.66	-6.52	4.97	-11.36
DAY 165	TIME 000	DIST 1.46	CUM UIST 3.04	SPEED 11.59	01R 148.4	260 CUM SPEED 37.02	2604 STT DRIFT CUM D DIR 2 145.6 6	1FT U 6•08	, 78.6-	06°02	CUM V
	9					or	ATT W/O W	* U * 3			
SPEFO	NORMAL UKIFI SPEFN DIR U		>	9.22	167.4	33.04	97.8	2.00	00.6-	15,62	-28.54
4.00	4.00 126.5	3.22	-2.38			Q	DIFFERFNCES	۳.			
				6.73	190.4	21.22	113.2	-1.22	-6.62	7.75	-17.98

Table 3.—Comparison with IIP Current File (BTT 02604).

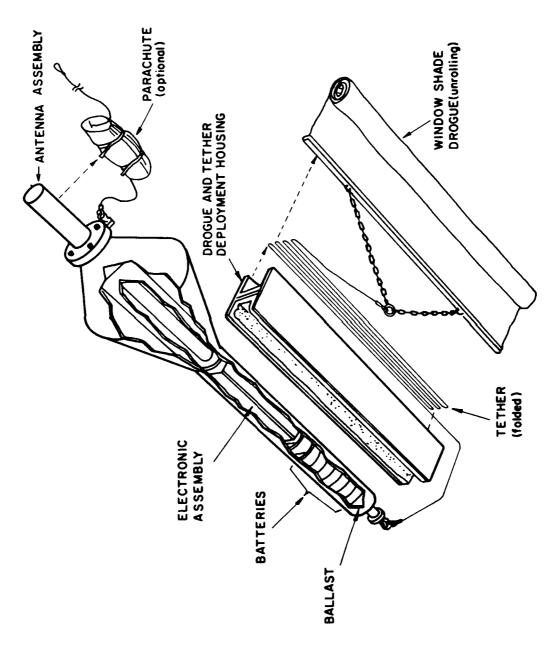


Figure 1.-BTT in TIROS Oceanographic Drifter configuration.

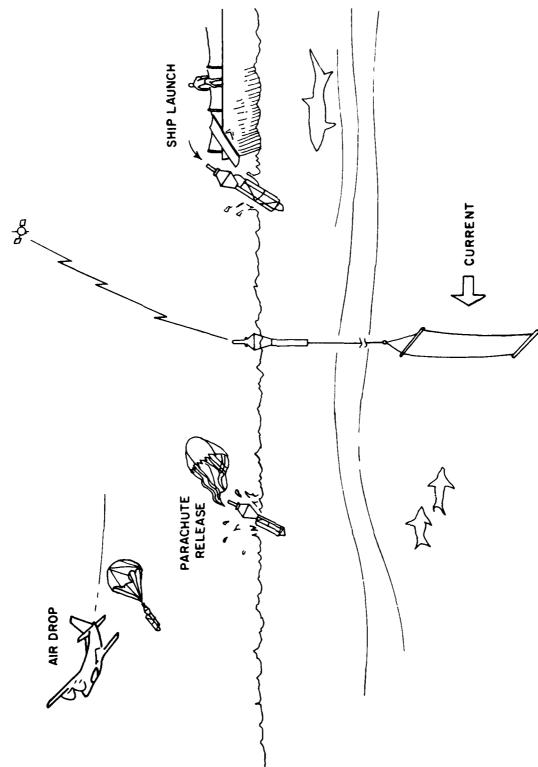


Figure 2,-BTT Deployment

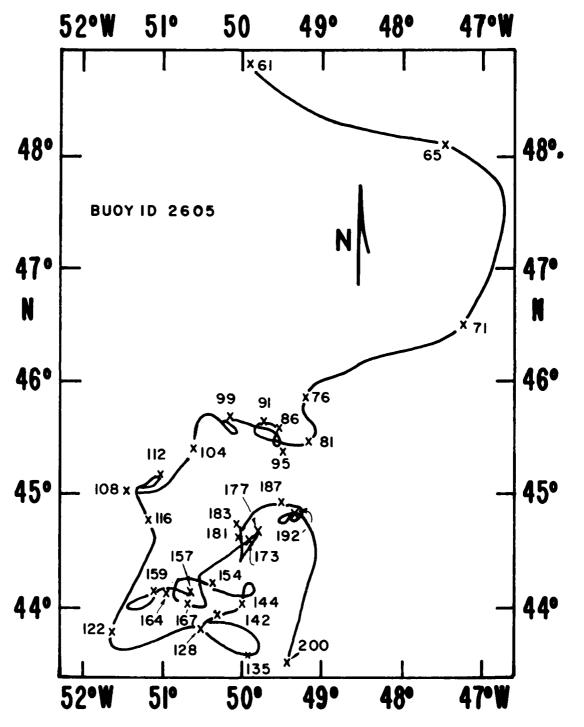
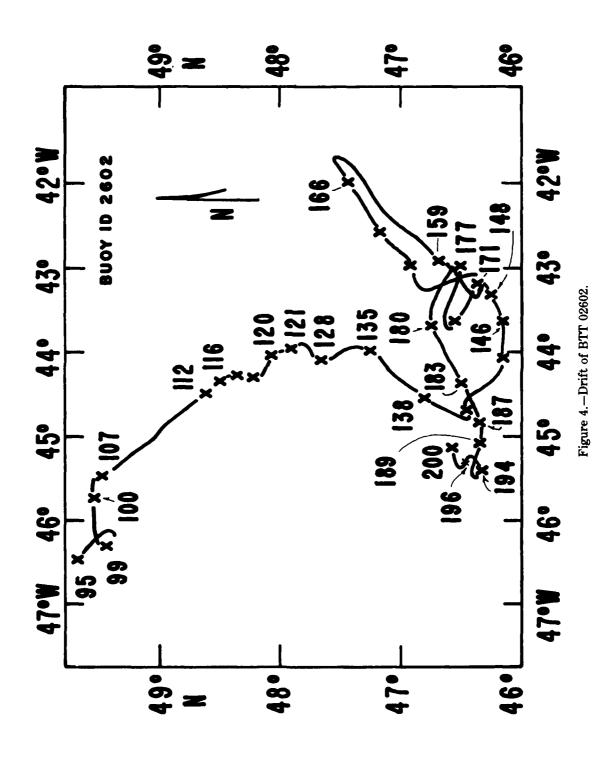


Figure 3.-Drift of BTT 02605.



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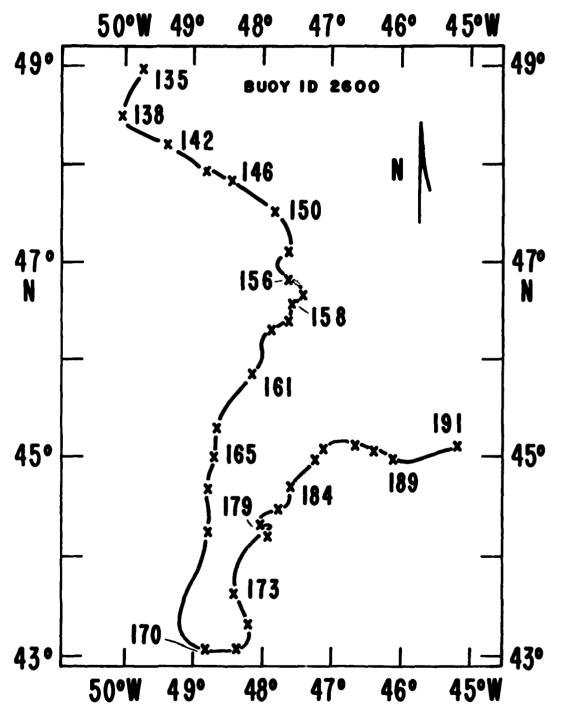
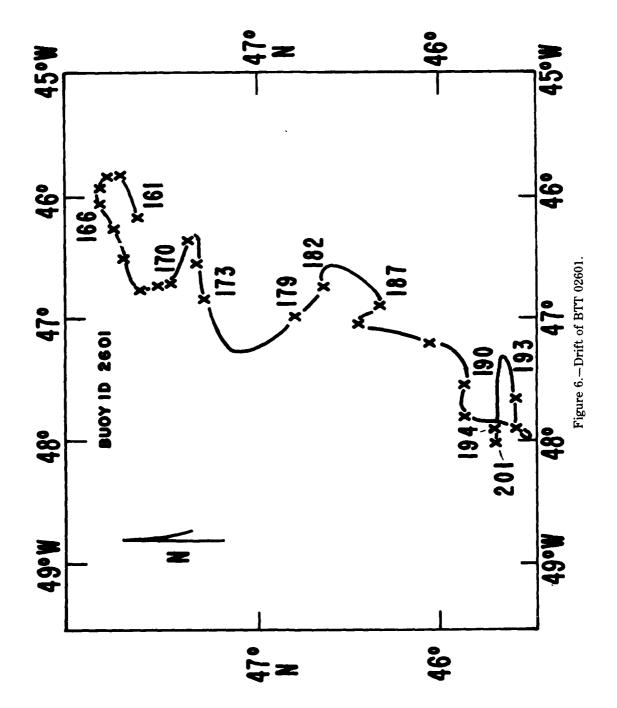
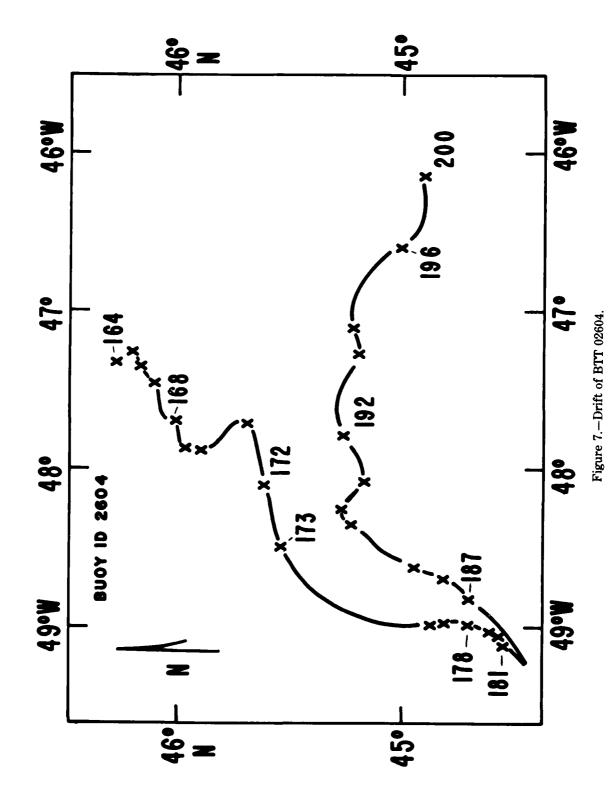


Figure 5.—Drift of BTT 02600.





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APPENDIX A IIP CURRENTS

				52.00 41.20 119 18
				52.00 41.00 116 15
LAT	LONG	DIR	CDD	52.00 40.40 116 15 52.00 40.20 116 15
LAI	LUNG	תוע	SPD	52.00 40.00 116
	_			52.00 39.40 116 15
LAT	LONG	NIB	SPN	52.00 39.20 116 15
52.00	57.00	0	n	52.00 39.00 116 15
52.00	56.40	0	. 0	51.40 57.00 0
52.00	56.20	0	n	51.40 56.40 J 0
52.00	56.00			51.40 56.20 0 0
52.00	55.40	1)	<u>n</u>	<u>51.40 56.00 0 0 0 </u>
52.00	55.20 55.00	0	<u> </u>	51.40 55.40 0 0
52.00	54.4n	160	. 53 . 53	51.40 55.20 0 0
52.00	54.21	150	23	51.40 55.00 160 23 51.40 54.40 160 23
52.00	54.00	150	23	51.40 54.40 160 23 51.40 54.20 160 23
52.00	53.40	160	23	51.40 54.00 160 23
52.00	53.20	150	23	51.40 53.40 160 23
52.00	53.00	150	23	51.40 53.20 160 23
52.00	52.40	160	23	51.40 53.00 23
52.00	52. 20	150	23	51.40 52.40 160 23
52.00	57.00	160	23	51.40 52.20 160 23
52.00	51.40	150	23	51.40 52.00 160 23
52.00	51.20 51.00	160	27 69	51.40 51.40 100 23
52.00	50.40	160 158	64	51.40 51.20 160 23 51.40 51.00 159 74
52.00	50.20	109	37	51.40 51.00 150 74 51.40 50.40 160 69
52.00	50.00	169	37	51.40 42
52.00	49.50	169	37	51.40 50.00 170 42
32.00	49.40	159	37	51.40 49.50 170 42
52.00	44.30	169	37	51.40 49.40 170 42
52.00	49,24	1~+	37	51.40 49.30 170 47
52.00	49.10	164	37	51.40 49.20 170 42
52.00	49.00	159	37	51.40 49.10 170 42
52.00	49.50	159	37	51.40 49.00 170 42
52.00	48.40	158	- 1 ₂	51.40 48.50 170 42
52.00 52.00	48.30 48.20	172 130	35 34	51.40 48.40 169 40
52.00	48.10	150	34	51.40 48.30 173 39 51.40 48.20 180 39
52.00	4 8.7 0	150	34	51.40 48.20 180 39 51.40 48.10 180 41
52.00	47.50	180	34	51.40 48.00 180 41
52.00	47.40	140	34	51.40 47.50 180 41
52.00	47.30	140	34	51.40 47.40 180 39
52.00	47.20	140	34	K1.40 47.70 180 39
52.00	47.10	140	34	51.40 47.20 190 37
52.00	47.00	180	34	51.40 47.10 180 37
52.00	46.50	172	35	51.40 47.00 180 37
52.00	46.40	168 158	35 35	51.40 46.40 172 37 51.40 46.40 179 37
52.00	46.20	168	35	51.40 46.40 159 37 51.40 46.30 169 37
52.00	46.10	165	36	51.40 46.20 169 37
52.00	46.00	161 =	36	41.40 46.10 165 3A
52.00	45.40	161	36	51.40 46.00 161 36
52.00	45.20	149	35	51.40 45.40 150 37
52.00	45.00	140	36	51.40 45.20 140 36
57.00	44.40	140	36	51.40 45.00 129 34
52.00	44.20	140	36	51.40 44.40 129 36
57.00	44.05	129	34	51.40 44.20 124 34
52.00 52.00	43.40	159	36 36	51.40 44.00 129 36
52.00	43.00	154	36 36	51.40 43.40 119 37
52.00	47.40	IŠE	-20	51.40 43.20 119 37 51.40 43.00 121 35
52.00	42.20	118	29	51.40 42.40 118 24
52.00	42.00	iia		51.40 42.20 11H 29
52.00	41.40	119	18	51.40 42.00 119 1H

NOTE: LAT LONG ARE IN DEGREES.MINUTES.

LAT	LONG	DIR	SPD					
51.40	41.40	119	13	51.20	42.00	47	1.3	
51.40	41.20	116	15	51.20	41.40	97 97	1 A 1 B	
51.40	41.00	1 11 4	14	51.20	41.20	·— ·- 99 ·	14	
51.40	40.40	1.18	1 4	51.20	41.00	99	14	
51.40 51.40	40.20	1	14	51.20	40.40	99	14	
51.40	39.40	103	14	51.20	40.20	99	14	
51.40	39.20	108	14	51.20 51.20	40.00 39.40	99	14	
51.40	39.00	ins	14	51.20	34.20	. 99	14 14	
51.20	57.00	0	9	51.20	39.00	ųq	14	
51.20	56.40	n	n i	51.00	57.00	0	0	
51.20	56.20			51.00	56.41)	<u> </u>	<u> </u>	
51.20	56.00 55.40	U U	0	51.00	56.20	0	n	
51.20	55.20	150	23	51.00	56.00	0	n	
51.20	55.00	150	23	51.00 51.00	55.40 55.20	0 160	9 3	
51.20	~4.40	150	23	51.00	55.0n	150	23 23	
51.20	54.2n	100	23	51.00	54.40	160	24	
71.2)	54.00	160	23	51.00	54.20	150	23	
51.2)	53.47	100	23	51.00	54.00	150	23	
51.20	~3.2n	167	23	51.00	53.40	160	23	
51.20 51.20	53.00 52.40	167	23	51.00	53.20	160	23	
51.20	52.2n	150 150	23 23	51.00 51.00	53.00	150	23	
51.20	-5.70		53	51.00	52.40	150	23	
51.20	51.40	150	23	51.00	52.00	150 150	23	
51.20	-1.20	160	23	51.00	51.40	160	23	
51.20	71.00	100	76	51.00	51.20	150	23	
61.21	P 11 * * U	1-9	74	51.00	51.00	149	78	
51.20	P.11. 5 U	17.5	42	51.00	50.40	160	76	
51.20 51.20	-n.un	170	42	51.00	~n.5v	171	44	
51.27	44.51 49.47	170 170	42 42	51.00	50.00	171	44	
51.20	44.30	175	42	51.00 51.00	49.50 49.40	171	44	
51.20	49.20	170	42	51.00	49.30	171 171	4 4 4 4	
51.20	49.11	179	42	51.00	49.20	171	44	
51.20	49.00	170	42	51.00	49.10	171	44	
51.20	44.50	170	42	51.00	49.00	171	44	
51.27	48.40	169	4 0	51.00	4 ዓ. 5ኅ	171	44	
51.20 51.20	48.30 45.30	173	30	51.00	49.40	171	44	
51.20	4A.20 49.10	130 150	39	51.00	4P.30	171	44	
51.20	48.0n	130	41	51.00	4H.20 4H.IO	171 173	44	
51.29	47.50	1 - 0	41	51.00	48.0h	140	41	
51.27	47.41	140	30	51.00	47.50	180	39	
51.20	47.30	130	39	51.00	47.40	180	37	
51.20	47.21	180	37	51.07	47.31	180	77	
51.20	47.10	140	37	51.00	47.20	180	34	_
51.20 51.20	47.00	1 40	37	51.00	47.10	180	74	
51.27	48.50 48.40	172 159	37 3 7	51.00	47.00	140	34	
71.20	46.31	155	3.4	51.00 51.00	46.51 46.41	172 168	35 35	
51.20	46.20	151	36	51.00	46.30	165	36	
51.20	46.10	154	34	51.00	46.20	160	34	
51.20	45.00	[50]	37	51.00	46.10	153	36	
51.20	45.40	140	36	51.00	46.00	148	35	
51.20	45.20	129	34	51.00	45.40	148	34	
51.20 51.20	45.00 44.40	119	37	51.00	45.20	137	34	
51.20	44.20	119 119	37 37	51.00	45.00	137	34	
51.20	44.00	119	37	51.00 51.00	44.40	121	36 35	
51.20	43.40	100	37	51.00	44.00	109	34	
51.20	43.20	100	37	51.00	43.40	109	74	
51.20	43.00	100	37	51.00	43.20	101	35	
51.27	42.41	94	30	51.00	43.00	98	30	
51.20	42.20	44	30	51.00	42.40	97	18	

LAT	LONG	DIR	SPD					
51.00	42.20	97	19	50.40	42.40	47	18	
51.00	42.00	97	19	50.40	42.20	97	18	
51.00	41.40	99	14	50.40	42.00	Ý0	50	
51.00	41.20	94	14	50.40	41.40	40	13	
51.00	41.00	99	14	50.40	41.20	40	13	
51.00	40.40	44	14	50.40	41.00	40	13	
51.00	40.20	99	14	50.40	40.40	70	13	
51.00	40.00	44	14	50.40	40.20	40	13	
51.00	34.40	49	1 4	50.40	40.00	→ ()	13	
51.00	34.20	44	14	50.40	34.40	٠, ١	13	
51.00	39.00	44	14	50.40	30.20	₩ n	13	
50.40	57.00	0	1	50.40	39.00	<u> </u>	13	
50.40	56.40	-0	<u></u>	50.20	57.00	_C		
50.40 50.40	56.20 ≒6.00	0	0	50.20	56.40	Ú	n	
50.40	55.41	0 160	23	50.20	56.20	1)	u u	
50.40	55.20	160	23	50.20 50.20	56.00 55.40	0 150	23	
50.40	55.00	150	23	50.20	55.20	150	23	
50.40	54.40	151	23	50.20	57.00	150	23	
50.40	54.20	150	23	50.20	54.40	160	23	
50.40	54.00	150	23	50.20	54.20	150	23	
50.40	53.40	160	23	50.20	54.00	150	23	
50.40	53.20	150	23	50.20	53.40	150	23	
50.40	53.00	15 -	23	50.20	53.20	160	23	
50.40	52.40	150	23	50.20	53.00	160	23	
50.40	52.20	156	23	50.20	52.40	160	23	
50.40	52.00	150	23	50.20	42.20	157	23	
50.40	51.40	150	23	50.20	52.00	160	23	
50.40	51.20	150	23	50.20	51.40	160	23	
50.40	51.00	150	23	50.20	51.20	167	23	
50.40	50.20	149	74 76	50.20	51.00	150	24	
50.40	50.00	150 135	32	50.20	50.40 50.20	150	9 N 5 N	
50.40	49.51	135	32	50.20 50.20	50.00	150 135	32	
50.40	49.40	135	32	50.20	49.50	135	32	
50.40	44.30	135	38	50.20	49.40	135	32	
50.40	49.21	135	32	50.20	49.30	135	32	
50.40	49.10	135	32	50.20	44.20	135	32	
50.40	49.00	135	32	50.20	49.10	135	32	
50.49	48.50	135	32	50.20	49.00	116	34	
50.40	48.40	135	32	50.20	4P.50	90	1 4	
50.40	44.30	135	32	50.20	44.40	90	11	
50.40	48.20	135	32	50.20	4H.3n	90	11	
50.40	48.10	135	32	50.20	44.20	40	11	
50.45	48.00	135	35	50.20	49.10	3 0	11	
50.40 50.40	47.50 47.40	135	32	50.20	48.00	911	11	
50.40	47.30	135	32 32	50.20	47.50	3 0	11	
50.40	47.20	135	35	50.20	47.40	90	11	
50.40	47.10	135	32	50.20	47.30	40	11	
50.40	47.00	135	32	50.20	47.10	90	11 11	
50.40	46.50	135	32	50.20	47.00	40	11	
50.40	46.40	135	32	50.20	46.50	90	ii	
50.40	46.30	135	32	50.20	46.40	90	ii	
50.40	46.20	135	32	50.20	46.30	90		
50.40	46.10	1 35	32	50.20	46.20	40	23	
50.40	46.00	140	33	50.20	46.10	90	27	
50.40	45.40	154	33	50.20	46.00	40	30	
50.40	45.20	129	33	50.20	45.40	131	71	
50.40	45.00	120	32	50.20	45.20	120	32	
50.40	44.40	150	12	50.20	45.00	115	30	
50.40	44.20 44.00	111	32	50.20	44.40	112	30	
50.40 50.40	44.00	111 10a	35 29	50.20	44.20	112	30	
50.40	43.20	98	30 30	50.20	44.00	112	30	
50.40	43.00	3 8	30	50.20 50.20	43.40	98 98	30	
· ·		- 1 -		10 0 E U	43.20	777	30	

LAT	LONG	DIR	SPD					
50.20	43.00	98	30	50.00	43.20	90	32	
50.20	42.40	90	20	50.00	43.00	90	27	
50.20 50.20	42.20	40	50 50	50.00 50.00	42.40 42.20	90 90	50	
50.20	41.40	- 40	13	50.00	42.00	40	20	
50.20	41.20	90	13	50.00	41.40	- 40	20	
50.20	41.00	90	13	50.00	41.20	90	20	
50.20	40.40 40.20	9 <u>0</u>	13	50.00	41.00	90	20	
50.20	40.00	30	13	50.00	40.20	90	50	
50.20	39.40	40	1 3	50.00	40.00	95	19	
50.20	39.20	40	Su	50.00	39.40	78	23	
50.00	57.00	0	0	50.00 50.00	39.20 39.00	78 78	23 23	
50.00	56.40	<u>0</u>	<u> </u>	49.40	57.00	0		
50.00	56.20	0		49.40	56.40	0	<u> </u>	
50.00 50.00	56.00 55.40	n ')	0	49.40	56.20	0	0	
50.00	55.20	0	<u>0</u>	49.40	56.00 55.20	0	0	
50.00	55.00	160	23	49.40	55.40	ŏ	ő	
50.00	54.40	160	23	49.40	55.00	0	0	
50.00	54.20 54.00	- <u>160</u>	<u>23</u>	49.40	54.40	0	<u> </u>	
50.00	53.40	150	23 23	49.40	54.20 54.00	139	39	
50.00	53.20	160	23	49.40	53.40	149	45	
50.00	53.00	160	23	49.40	53.20	159	54	
50.00	52.40	160 160	23	49.40	53.00	159	53	
50.00		160	23	49.40	52.40	160	23	
50.00	51.40	160	23	49.40	52.00	160	23	
50.00	51.20	160	23	49.40	61.40	160	23	
50.00 50.00	51.00 5.0040	160 160	53	49.40	51.20	160	23	
50.00	50.20	150	#U #	49.40 49.40	50.40	160 160	23 _#	
50.00	-50.04	. I=0	80 *	49.40	50.20	150	70 *	
50.00	49.50	113	33 *	49.40	50.00	150	мо "	
50.00	49.40	102	27** 34 *	49.40	49.50 49.40	150 103	A0 * 1A *	
50.00	49.2 n -	126	45%	- 49.40	49.30	42	17#	
50.00	44.10	137	42 🚆	49.40	49.20	166	31 #	
50.00	49.00	103	16 *	49.40	49.10	171	44 *	
50.00	48.50 48.40	12	20 *	49.40	49.00 48.50	170 94	45	
50.00	48.30	Û	10 *	49.40	48.40	2	14*	
50.00	4R.20	- 2	11.*	49.40	48.3n	357		
50.00	48.10	351	15 *	49.40	48.20	358	Ω#	
50.00 50.00	47.50	342 = - 349	" ∏1⊊"" 3 °	49.40	44.10 44.00	342 340	13#	
50.00	47.40	118		49.40	47.50	340	16.5	
50.00	47.30	127	<u>۲</u> *	49.40	47.49	328	9 2	
50.00 50.00	47.20 47.10	113 71	д * - 14 *	49.40	47.30	28.	10*	
50.00	47.00	78	74 *	49.40	47.20 47.10	- 1	5 ′*	
50.00	46.50	54	37 #	49.40	47.00	10	36#	
50.00	46.40	33	56 *	49.40	46.50		34#	
50.00 50.00	46∙30 ~46∙20	13 352	54 3A ★	49.47	46.40	5	19#	
50.00	46.10	215	1# *	49.40	46.30 46.20	259 227	26 ±	
30.00	46.00	238	20 🛣	49.40	46.10	551	35# 35#	
50.00	45.40	231	33 *	49.40	46.00	250		
50.00 50.00	45.21 45.00	935	2A #	49.40	45.40 45.20	225 198	27# 22#	
50.00	44.40	171	32 *	49.40	45.00	7.40		
50.00	44.20	94	32	49.40	44.40	171	32	
50.00	44.00	9ē	72	49.40	44.20	90	34	
50.00	43.40	94	32	49.40	44.00	90	34	

LAT	LONG	DIR	SPD					
49.40	43.40	90	30	49.20	44.00	79		
49.40	43.20	90	30	49.20	43.40	ei	37 30	
49.40	43.00	40	30	49.20	43.20	81	30	
49.40	42.40		S0	49.20	43.00	81	30	
49.40	42.00	90 90	20 20	49.20	42.40	82	18	
49.40	41.40	70	50	49.20	42.20	- 82	18	
49.40	41.20	40	20	49.20	41.40	82	18 18	
49.40	41.00	42	18	49.20	41.20	H2	18	
49.40 49.40	40.40	32] a	49.20	41.00	82	18	
49.41	40.20 40.00	45	14	49.20	40.40	42	18	
49.40	39.41		<u>21</u>	49.20	40.20	85	18	
49.49	34.20	78	23	49.20 49.20	40.00	×2] 4	
49.40	39.00	78	23	49.20	39.40	<u>78</u>	23	
49.20	57.00	0	0	49.20	39.00	78	23 23	
49.20	-6.40	υ	0	49.00	57.00	·		
49.20	56.20	0	0	49.00	56.40	0	n	
44.50	55.40	0	0	49.00	56.20	0	0	
66.20	55.20	-'n'	· · - · · · · · · · · · · · · · · ·	49.00	56.00	0	0	
49.20	55.00	Ö	'n	49.00	55.40	0	0	
49.20	4.40	ŏ	ń	49.00	55.20 55.00	0		
49.20	54.20	n	n	49.00	54.40	0	0	
49.71	-4.00	0	0	49.00	54.20			
44.20	53.40	0	0	49.00	54.00	Ó	ñ	
49.20 49.20	53.20 53.00	145	45	49.00	53.40	0	0	
49.20	· 2.40	- 160 160	49	49.00	53.20	149	45	
49.20	52.20	150	23	49.00	53.00	160	49	
49.21	32.00	160	- 23	49.00	52.40	160	49	
44.27	51.40	155	34 *	49.00	52.00	160	53 53	
49.20	51.20	124	30 *	49.00	51.40	128	23 *	
49.20	51.00	ລາງ	15 👱	49.00	51.20	122	29 #	
49.20 49.20	50.40 50.20	104	24	49.TT	~I.00	127	55 *	
49.20	50.00	111	30 [™]	49.00	50.40	125	16	
49.20	49.50	157	80 *	49.00	50.20	150	14	
49.20	49.40	150	80 *	49.00	50.00 49.50	- 150 153	80.T 80 *	
49.20	49.30	173	37 *	49.00	49.40	153	60. *	
49.20	49.20	181	36 🕌	49.00	49.31	144	24 *	
49.20	49.10	170	30 "	49.00	49.20	140	33 ±	
49.20	49.00 48.50	137	55 *	49.00	49.10	136	36 #	
49.20	4F.40	- 40	· 18 **	49.00	49.00	126	31 ,,	
49.20	48.30	62	7 *	49.00	48.50	150	24	
49.20	45.20	6	4 *	49.00	48.40 48.30	142 158	25 *	
49.20	48.10	2	3 🛊	49.00	48.20	153	11 *	
49.20	48.00	24	l #	49.00	48.10	15	* #	
49.20 49.20	47.50 47.40	297	? *	49.00	48.00	5	5 #	
49.20	47.30	320 330	14 *	49.00	47.50	38	7 #	
49.20	47.20	- 352	16 * =	49.00	47.40	25	7	
49.20	47.10	342	18 *	49.00	47.30 47.20	11 355	12 7 #	
49.20	47.00	317	19#	49.00	47.10	286	- (; -	
49.20	45.50	241	21 * 25 *	49.00	47.00	286	9 #	
49.20 49.20	46.49	271	25 *	49.00	46.50	294	Iń#	
49.20	46.20	256 249	<0 ₩	49.00	46.40	275	9 🚜	
49.20	46.10	249 246	23 *	49.00	46.30	240	10 #	
49.20	46.00	246	15 *	49.00	46.20	219	14	
49.20	45.40	200	22 *	49.00	46.00	218	16 11 *	
49.20	45.20	210	13 *	49.00	45.40	185	9 *	
44.20 49.20	45.00	0	0.4	49.00	45.20	108	22 *	
49.20	44.20	225 90	26	49.00	45.00	87	50 *	
	77861	70	37	49.00	44.40	90	37	

LAT	LONG	DIR	SPD					
49.00	44.20	90	37	48.40	44.40	100	2.4	
44.00	44.00	79	37	48.40	44.20	÷0	37 37	
49.00	47.40	79	37 ⁻	48.40	44.00	79	37	
49.00	43.20	79	37	48.40	43.40	69	39	
44.00	43.00	40	30	4A.40	43.20	59	40	
49.00	42.40	<u>68</u>	25	46.40	43.00	59	4.0	
49.00 49.00	42.20 42.00	6H	56	4A.40	42.40	51	29	
49.00	41.40	68 79	25 26	48.49 48.49	42.20	60	23	
49.00	41.20	79	26	48.40	42.00 41.40	58	25	
44.00	41.00	79	26	48.40	41.20	71 71	29	
49.00	40.40	42	19	48.40	41.00	81	29 30	
49.00	40.20	45	14	44.49	40.40	+2	14	
49.00	40.00	42	18	48.40	40.20	нŽ	i e	
49.00	39.40	79	26	4H.40	40.00	42	19	
49.00 49.00	39.20 39.00	79 79	56	48.40	39.40	91	30	
48.40	57.00	0	0 54	48.40 48.40	39.20	~1	30	
48.40	56.40	 0	0	48.20	39.00 57.00	<u> </u>	30	
48.40	56.20	0	ñ	48.20	56.40	0	0	
4 H . 4 O	56.00	0	n	48.20	56.20	. 0	<mark>0</mark>	
48.40	55.40	0	n	48.20	56.00	ě	'n	
48.40	55.20	0	U	44.20	55.40	0	n	
49.40	55.00	U	0	48.20	55.20	0	n	
48.40 48.40	54.40 54.20	0	0	48.20	55.00	0	n	
48.40	54.00	-) (i	n n	4H.20	54.40	0	0	
48.43	53.40	'n	n	48.20 48.20	54.20 54.00	0	n	
48.40	~3.20	0	0	48.20	53.40	0	n n	
44.40	53.00	134	39	48.20	53.20	n n	0	
48.40	F2.40	150	49	4A.20	53.00	139	39	
48.40	52.20	169	49	48.20	52.40	160	49	
48.40	55.00	1=0	4 H	48.70	5 2. 20	169	49	
4H.40 48.49	51.40 51.20	115 134	14 *	46.20	52.00	1 H O	4 14	
48.40	51.00	113	21 *	48.20 48.20	51.40 51.30	180	13	
48.40	50.40	115	30 *	4A.20	51.20	116	2 * 5 * -	
48.40	50.20	155	33 *	48.20	50.40	117	5 # 17 #	
48.40	50.00	127	3 ← ★	48.20	Kn.20	117	24 *	
48.41)	49.50	130	40 *	44.20	50.00	104	2A 🛣	
48.40	49.40	138	A() *	48.20	49.50	101	34 🚆	
48.40	49.30	1.35	80 *	48.20	49.40	118	44 *	
48.40	49.2n 49.1n	134 129	33 *	48.20 48.20	49.30	130.	57 *	
48.40	49.00	141	23 * 25 *	4A.20	49.20 49.10	131 130	61 *	
48.40	48.50	154	3n *	48.20	49.00	128	57 # 52 #	
48.40	44.40	158	* وح	48.20	48.50	124	40 *	
44.40	49.30	151	26 *	46.50	48.40	121	40	
48.40	40.20	135	21 *	48.20	48.30	117	- A .: *	
48.40 48.40	48.10 48.00	115	16 *	48.20	48.20	103	41 *	
48.40	47.50	101 84	12 *	48.21 48.20	4R.10	93	40 **	
48.40	47.40	41	€#	48.20	48.00 47.50	100	40*	
48.40	47.30	46	5 *	48.20	47.40	108 105	43# 41 #	
4A.40	47.20	198	1 *	48.20	47.30	98	41 * 34 *	
48.40	47.10	185	6 *	48.20	47.20	9Ř	56.	
48.40	47.00	186	3 *	4 8. 27	47.10	100	- 24* 24* 22*	
48.40 48.40	46.50 46.40	326	1 *	48.20	47.00	96	22 <u>#</u>	
4H.40	46.40 45.30	251 189	1 *	48.20 48.20	46.50	93	TAT	
48.40	46.20	155		48.20	46.30	102	15#	
48.40	46.10	49	5 *	48.20	46.20	111	12#: A#	
48.47	45.00	79	7 **	48.20	46.10	74		alle at a
4A.40	45.40	12	21 *	48.20	46.00	115	ıí."	
4P.40	45.20	43	22 *	48.20	45.40	50	11" 7#. 20#	
48.40	45.00	76	S2 *	48.20	45.20	1	20 *	

48.20							
	45.00	24	20 #	48.00	45.20	17	16 *
48.20	44.40	100	37	48.00	45.00	137	34
4A-20	44.20	40	37	48.00	44.40	109	34
48.20	44.00	79	37	48.00	44.20	40	34
4A.20	43.40	70	42	48.00	44.00	71	29
48.20	43.20	70	42	48.00	43.40	50	36
48.20	43.00	70	42	48.00	43.20	50	36
48.20 48.20	42.40 42.20		29 23		43.00	50	36
48.20	42.00	60	23	48.00	42.40	51	29
44.20	41.40	- 51	23	48.00	42.20	61	29
46.20	41.20	61	24	48.00 48.00	42.00 41.40	↑1 71	29
48.20	41.00	71	30	48.00	41.20	71	29
48.20	40.40	42	14	48.00	41.09	71	29
48.20	40.20	42	18	48.00	40.40	- 56	17
48.20	40.00	42	18	48.00	40.20	56	17
48.20	39.40	78	35	48.00	40.00	66	17
48.20	39.20	78	35	44.00	39.40	77	21
48.20	39.00	78	35	48.00	39.20	77	21
48.00	57.00	0	n	48.00	39.00	77	21
48.00	-6.40	n	n	-47.40	57.00	0	<u> </u>
48.00	56.20	Ü	n	47.40	56.40	()	n
48.00	~6.00	ń	n	47.40	56.20	0	· • •
48.00	55.40	0	<u> </u>	47.40	56.00	0	_ ^
48.00	22.50	e	n	47.40	55.40	0	0
48.00	55.00	0	0	47.40	55.20	0	0
48.00	-4.40	o.	n	47.40	55.00	0	, N
44.00	54.20	9	n	47.40	54.40	0	0
4A.00 44.00	-4.00	0	0	47.40	54.20	- · · n	
4A.00	53.40	<u> </u>	0	47.40	54.00	0	
48.00	53.20 53.00	ີ ປ	0	47.40	53.40	7	0
48.00	~2.40	171	44	47.40	53.20		·
48.00	52.20	169	49	47.40	E3.00		40
48.00	-2.00	190	40	47.40 47.40	52.40 52.20	169 TEN	
48.00	51.40	220	23	47.49	52.00	199	49
48.00	51.20	206	10	47.40	51.40	199	23
48.00	51.00	206	10 *	47.40	51.20	188	23
48.00	50.40	153	10 *	47.40	51.00	180	23
48.00	50.20	169	7 *	47.40	50.40	171	7
48.00	50.00	9.0	٠.	47.40	50.20	326	* · · · = · · · · ·
48.00	49.50	104	7 *	47.40	50.00	302	i *
48.00	49.40	134	10 *	47,40	49.50	195	12 *
48.00	49.30	139	17 *	47.40	49.40	194	12 #
48.00	49.20	129	24	47.40	49.30	224	
44.00	49.10	155	35 *	47.40	49.20	243	7 *
4A.00	49.00	120	44 *	47.40	49.11	24R	5.4
48.00	44.50	119	49 #	47.40	49.00	223	
4H.00	48.40	114	52 *	47.40	48.50	156	4
48.00	48.30	108	57 *	47.40	48.40	95	7 #
48.00	4A.20	104	59 *	47.40	4A.3h	B1	7 *
48.00 48.00	48.10	101	57 ±	47.40	48.20	110	10#
48.00 48.00	48.00 47.50	96 45	53 T	47.40	48.17	134	15*
48.00	47.40	109	49*	47.40	48.00	143	22
48.00	47.30	163	52 *	47.40	47.50	146	2A * 32 *
48.00	47.20	129	48 #	47.40 47.40	47.40 47.30	151 161	
48.00	47.10	132	30	47.40	47.20	171	35 " 44 #
48.00	47.00	141	30 #	47.40	47.10	178	40#
48.00	46.50	156		47.40	47.00	181	44 #
48.00	45.40	171	33****	47.40	46.50	181	35#
48.00	45.30	142	1A #	47.40	46.40	176	26
48.00	46.20	210	4 #	47.40	46.30	164	
							15 * 7 *
	46.10	343	× **	6 7 ± & U		97	
48.00	46.10	343 359	я# 6#	47.40 47.40	46.20	97 45	15

LAT	LONG	DIR	SPD					
47.40	45.40	68	14 #	47.20	45.00	33	19 *	
47.40	45.20	43	7 4	47.20	45.40	89	2 #	
47.40	45.00	149	32	47.20	45.20	24	5 #	
47.40	44.40	120	32	47.20	45.Q0 44.40	323	<u>^ </u>	
47.40	44.00	81	35	47.20	44.20	131	24	
47.40	43.40	59	32	47.20	44.00	90	27	
47.40	43.20	<u> </u>	31	47.20	43.40	52	26	
47.40 47.40	43.00 42.40	50	33	47.20 47.20	43.20 43.00	41 37	24 26	
47.40	42.20	50	33	47.20	42.40	39	34	
47.40	42.00	50	33	47.20	42.21	39	36	
47.40	41.49	48	24	47.20	42.00	39	34	
47.40	41.27	48 48	24	47.20	41.40	41	24	
47.40	40.40	49	21	47.20	41.00	41	24	
47.40	40.20	60	18	47.20	40.40	40	21	
47.40	40.00	<u> </u>	18	47.20	40.20	40	21	
47.40 47.40	39.40 39.20	50	23	47.20 47.20	40.00 39.40	48	21 24	
47.40	39.00	50	23	47.20	39.21	4H	24	
47.20	57.00	0	0	47.20	39.00	4.8	24	
47.20	56.40	0	0	47.00	57.00	0	<u></u>	
47.20	56.20	<u> </u>	<u> </u>	47.00	56.40	0	<u> </u>	
47.20	55.40	ŏ	n	47.00	56.00	Ö	ő	
47.20	55.20	0	0	47.00	55.40	0	n	
47.20	55.00	0	0	47.00	55.20	0	0	
47.20 47.20	54.40 54.20	0	0	47.00 47.00	55.00 54.40	0	0	
47.20	54.00	- 		47.00	54.20	- 6 -		
47.20	53.40	0	0	47.00	54.00	0	0	
47.20 47.20	53.20	7	0	47.00	53.40	0	0	
47.20	53.00 -2.40	- O	44	47.00	53.20	0 -	0	
47.20	52.20	199	49	47.00	52.40	209	47	
47.20	52.00	199	49	47.00	52.20	210	51	
47.20	51.40	199	23	47.00	52.00	199	49	
47.20	51.20 51.00	188 180	23 23	47.00 47.00	51.40	191	23 23	
47.20	50.40	169	23	47.00	51.00	180	23	
47.20	50.20	169	23	47.00	50.40	180	23	
47.20	50.00	231	я #	47.00	50.20	169	23	
47.20	49.50	241 187	- A *	47.00 47.00	50.00 49.50	169	53	
47.20	49.30	151		47.00	49.40	180	23	
47.20	49.20	170		47.00	49.30	180	23	
47.20	44.10	152	3 #	47.90	49.20	180	30	
47.20 47.20	49.00 48.50	100 158	2 #	47.00 47.00	49.10 49.00	184 188	30 30	
47.20	4R.40	231	16	47.00	48.50	192	31	
47.20	48.30	193	10 👱	47.00	48.40	198	29	
47.20	49.20	224	17 =	47.00	48.3h	19A	29	
47.20	48.10 48.00	240 355	- 5 * -	47.00	48.20 48.10	50	18 * 17	
47.20	47.50	59	4 *	47.00	48.00	91	14 *	
47.20	47.40	163	25 #	47.00	47.50	158	14.8	
47.20	47.20	170	5? #	47.00	47.40	154	23 +	
47.20	47.10	170 165	58 # 51 #	47.00 47.00	47.30	161	46 # 58 #	
47.20	47.00	145	40	47.00	47.10	166	67	
47.20	46.50	160	24 ::	47.00	47.00	172	75.*	
47.20	46.40	159 125	10 *	47.00 47.00	46.50	177	53 * 27 *	
47.20	45.20	44	16 #	47.00	46.40	337	0 #	
47.20	46.10	27	26 #	47.00	46.20	357	9 #	

LAT	LONG	DIR	SPD					
47.00	46.10	337	д #	46.40	46 20	354	_ *	
47.00	46.00	276	7 🗰	46.40	46.20 46.10	354 351	7 * 6 *	
47.00	45.40	232	13 #	46.40	46.00	236		
47.00	45.20	254	13 * 13 *	46.40	45.40	217	5 *	
47.00	44.40	158	15	46.40	45.00	274 306	2 * 6 *	
47.00	44.20	100	3.6	46.40	44.40	31	7 *	
47.00 47.00	<u> </u>	90	<u> </u>	46.40	44.20	100	26	
47.00	43.20	59	37	46.40 46.40	44.00 43.40	90 68	30 32	
47.00	43.00	50	33	45.40	43.20	71	36	
47.00	42.20	50 50	36	45.40	43.00	50	37	
47.00	42.00	50 50	36 36	40.40 46.40	42.40 42.20	49	39	
47.00	41.40	3A	29	46.40	42.00	49	39	
47.00	41.20	38	29	46.40	41.40	50	36	
47.00 47.00	41.00	34 40	29 21	46.40	41.20	70	36	
47.00	40.20	40	21	46.40	41.00	61	19	
47.00	40.00	44	_ 21	45.40	40.20	49	21	
47.00 47.00	39.40 39.20	49	21	46.40	40.00	44	21	
47.00	39.00	47	21	46.40	39.4n 39.2n	51	14	
46.40	57.00	0	ŋ	46.40	34.00	51	14	
46.40	56.40		0	46.20	57.00	269	23	
46.40	55.20 56.00		<u> </u>	46.20	56.40	269	23	
46.40	55.40	ň	n n	46.20	56.20 56.00	269 269	23	
46.40	55.20	0		46.20	55.40	569		
46,40	55.00 54.40	<u>0</u>	0	46.20	55.20	269	23	
46.40	54.20	0	0	46.20 46.20	55.00 54.40	250	23	
46,40	54.00	0	<u> </u>	46.20	54.20	539	23	
46.40	53.40	0	0	46.20	54.00	228	23	
46.40	53.20 53.00	229	39	46.20 46.20	53.40	554	53	
45.40	52.40	250	39	46.20	53.20	231	23	
46.40	52.20	551	49	46.20	52.40	551	53	
46.40	52.00 51.40	210 149	51	46.20	52.20	510	23	
46.40	51.20	188	23	46.20	52.00 51.40	210 20#	23	
46.40	51.00	190	23	46.20	51.20	508	23 23	
46.40	50.40	190	23	46.20	51.00	501	24	
46.40	50.20	180 180	23	46.20	50.40	201	24	
46.40	49.50	144	23	46.20	50.20 50.00	190	23 23	
46.40	49.40	IRR	23	46.20	49.50	189	53	
46.40	49.30	168	23	46.20	49.40	188	23	
46.40	49.10	188	23 23	46.20 46.20	49.30	193 198	23	
46.40	49.00	217	154	46.20	49.10	198	23	
46.40	48.50	155	15#	46.20	49.00	184	4	
46.40	48.40	110 57	12.	46.20 46.20	48.50	514	6 *	
46.40	48.20	 		46.20	48.40	270 294	 -	
46.40	48.10	213	6*	46.20	48.20	233	5 #	
46.40	48.00	275	5 78	46.20	48.10	196	3 #	
46.40	47.40	303 179	21#	46.20	48.00 47.50	243 254	3 4	
46.40	47.30	185	65 m	46.20	47.40	208	10 # 52 #	
46.40	47.20	192	88 🐞	46.20	47.30	505	97	
46.40	47.10	200	79	46.20	47.20	201	103 "	
46.40	46.50	201	3A#	46.20 46.20	47.10	195	80 *	
45.40	46.40	195	15.	46.20	46.50	153	11 #	
46.40	46.30	321	0 🗰	46.20	46.40	75	9 .	

LAT	LONG	DIR	SPD				
46.20	46.30	58	14 #	46.00	46.40	68 #	15
46.20	46.20	61	17	46.00	46.30	50 #	16
46.20	46.10	76 115	16 # 16 #	46.00	46.20	43 *	14
46.20	45.40	155	15 *-	46.00	46.10	56 # 99 #	12
46.20	45.20	82	17*_	46.00	45.40	88 *	20
46.20	45.01	54	23 #	46.00	45.20	70 *	24
46.20 46.20	- 44.4n	63 74	35.#	46.00	45.00	67 *	21
46.20	44.00	57	37	46.00	44.20	18 * 68	46 25
46.20	43.40	47	30	46.00	44.00	71	79
46.20	43.20	71	36	46.00	43.40	68	3>
46.20	43.00 42.40	44	47	46.00 46.00	43.20 43.00	70	39
40.20	42.20	49	40	46.00	42.40	49	42 39
46.20	42.00	54	41	46.00	42.20	69	39
46.20 46.20	41.40	74 5.1	35	46.00	42.00	71	29
46.20	41.20	<u>58</u>	35 29	46.00	41.40	68	25
46.20	40.40	50	18	46.00	41.00	60	25 23
46.20	40.20	44	21	46.00	40.40	60	18
46.20 46.20	40.00	49	21	46.00	40.20	60	18
46.20	39.40 39.20	-1 51	14	45.00 46.00	40.00 39.40	49 51	21
46.20	39.00	1	14	46.00	39.20	41	14
46.00	57.00	254	23	46.00	39.00	51	14
46.00	56.40	2-9 254	23	45.40	57.00	259	49
46.00	56.20 56.00	2-4	- 23 -	45.40	56.40 56.20	259 259	23
46.00	55.40	254	23	45.40	56.00	259	23 23
46.00	55.20	7-4	23	45.40	55.40	259	23
46.00 46.00	55.00 54.40	254 250	23	45.40	55.20	259	23
46.00	54.20	240	23 23	45.40	55.00 54.40	259 250	73
46.00	54.00	228	23	45.40	54.20	240	23
46.00	53.40	231	23	45.40	54.00	228	23
46.00 46.00	43.20 53.00	218 218	23	45.40	53.40	220	23
46.00	52.40	210	23	45.40 45.40	53.20	518 518	23
46.00	52.20	210	23	45.40	52.40	219	23
46.00	52.00	210	23	45.40	52.20	220	23
46.00	51.20	20H	23	45.40	52.00	219	23
46.00	51.00	201	23	45.40 45.40	51.40 51.20	219 219	23 25
46.00	50.40	201	23	45.40	51.00	521	- 25
46.00	50.20	501	23	45.40	50.40	228	23
46.00 46.00	49.50	201 199	23	45.40	50.20	228	_ 23
45.00	49.40	198	23	45.40	50.00 49.50	231 225	23
46.00	49.30	204	23	45.40	49.40	218	23
46.00	49.20	208	23	45.40	49.30	510	23
46.00	49.10	<u>183</u>	10	45.40	49.20	177	12 #
46.00	48.50	178	11 #	45.40	49.10 49.00	137 164	17 # 10 #
46.00	48.40	166	4 #	45.40	48.50	171	
46.00	48.30	43	3 #	45.40	48.40	555	7 📅
46.00 46.00	48.20 48.10	177 208	1 # 14 #	45.40 45.40	48.30	237 226	23 * 63 *
46.00	48.00	215	31 #	45.40	48.10	555	87 *
46.00	47.50	217	70 📅	45.40	48.00	219	92 #
46.00	47.40 47.30	208	96 # 98 #	45.40	47.50	217	59 *
46.00	47.20	509	43 #	45.40	47.40	215 195	3A
46.00	47.10	559	A #	45.40	47.20	86	9 👼
46.00	47.00	64	6#	45.40	47.10	55	16**
46.00	46.50	82	12	45.40	47.00	41	17#

LAT	LONG	DIR	SPD					
45.40	46.50	45	16 #	45.20	47.00	73	22 *	
45.40	46.40	75	12 *	45.20	46.50	75	20 *	
45.40 45.40	46.30	109	10 *	45.20	46.40	94	16 *	
45.40	46.10		6	45.20	46.20	113	17 *	
45.40	46.00	14	6 *	45.20	46.10	97	14 #	
45.40	45.40	44	10*	45.20	46.00	74	12 *	
45.40 45.40	45.20	<u>79</u>	12 *	45.20	45.40	33	23 🖺	
45.40	44.40	63	39 *	45.20 45.20	45.20 45.00	51 40	23 * 38 *	
45.40	44.20	68	25	45.20	44.40	- 5	45 *	
45.40	44.00	71	29	45.20	44.20	68	25	
45.40	43.40 43.20	67 70	30 34	45.20	44.00	70	27	
45.40	43.00		··3 7	45.20 45.20	43.40	$\frac{71}{67}$	29	
45.40	42.40	71	22	45,20	43.00	68	30 32	
45.40	4ޕ20	71	55	45.20	42.40	71	25	
45.40	42.00	42	18 18	45.20	42.20	77	21	
45.40	41.20	45	18	45.20 45.20	42.00	92	18	
45.40	41.00	69	19	45.20	41.20	82 82	1A 1A	
45.40	40.40	60	18	45.20	41.00	69	19	
45.40 45.40	40.20	60 50	18	45.20	40.40	69	19	
45.40	39.40	51	18	45+20 45+20	40.20	60	_ 18	
45.40	39.20	51	14	45.20	39.40	60 51	18	
45.40	39.00	51	14	45.20	39.20	51	14	
45.20 45.20	57.00 56.40	259 259	49	45.20	39.00	51	14	
45.20	56.20	259 259	49 23	45.00	57.00	259	49	
45.20	56.00	259	53	45.00	56.40 56.20	259 259	49	
45.20	55.40	254	23	45.00	56.00	259	23	
45.20	55.2h 55.00	259	23	45.00	55.40	259	23	
45.20	54.40	259	23	45.00	55.20	259	23	
45.20	54.20	240	23	45.00 45.00	55.00 54.40	259 250	23 23	
45.20	54.00	551	23	45.00	54.20	240	23	
45.20	53.40 53.20	551	23	45.00	54.00	218	23	
45.20	53.00	219 219	23 23	45.00	53.40	220	23	
45.20	52.40	219	23	45.00 45.00	53.20 53.00	220 220	<u>23</u>	
45.20	52.20	219	23	45.00	52.40	219	23	
45.20	52.00	214	23	45.00	52.20	208	23	
45.20	51.40 51.20	208 209	23	45.00	52.00	208	23	
45.20	51.00	204	23	45.00 45.00	51.40 51.20	504	23	
45.20	50.40	209	23	45.00	51.00	209	23	
45.20	50.20 50.00	204	23	45.00	50.40	808	23	
45.20	49.50	209 213	23	45.00	50.20	510	23	
45.20	49,40	219	23	45.00 45.00	50.00 49.50	208	23 * -	
45.20	49.30	220	23 🚜	45.00	49.40	230	14 #	
45.20 45.20	49.20	178	. *	45.00	49.30	141		
45.20	49.00	134	17 *	45.00	49.20	144	*	
45.20	48.50	195	42 *	45.00 45.00	49.10	187 193	. 9 *	
45.20	48.40	206	90 ★	45.00	48.50	194	115 *	
45.20	48.30	211	106 *	45.00	48.40	198	108 #	
45.20	48.20 48.10	535	69 # 43	45.00	48.30	198	4A *	
45.20	48.00	249	19	45.00 45.00	48.20 48.10	1H2 46	13	
45.20	47.50	345	7 *	45.00	46.00	39	24 *	
45.20	47.40	38	17 +	45.00	47.50	40	27 *	
45.20	47.20	50 6 2	22. #	45.00	47.40	38	27 #	
45.20	47.10	71	23 #	45.00 45.00	47.30	46	27 #	
			- 4		- · • • •		LU 🖶	

LAT	LONG	DIR	SPD					
45.00	47.10	56	25 *	44.40	47.20	43	30*	
45.00	47.00 46.50	72 87	25 ∌ 24 #	44.40	47.10	50 64	27*	
45.00	46.40	93	?5 <u>.</u>	44.40	46.50	79	22×	
45.00	46.30	97	28 4	44.40	46.40	79	23*	
45.00	46.20	106	30 T	44.40	46.20	83 113	21 "	
45.00	46.00	94	22 *	44.40	46.10	129	29*	
45.00	45.40	50	20 #	44.40	46.00	120	28*	
45.00	45.20	<u> 26</u> 71	36 # 29	44.40	45.40 45.20	61	26 *	
45.00	44,40	71	29	44.40	45.00	19	41	
45.00 45.00	44.20	71 71	29	44.49 44.40	44.40 44.20	71 68	29 32	
45.00	43.40	71	59	44.40	44.00	71	36	
45.00	43.20	71	36	44.40	43.40	71	36	
45.00 45.00	43.00 42.40	68 78	37 35	44.40 44.40	43.20 43.00	70	39 42	
45.00	42.20	81	32	44.40	42.40	78	35	
45.00	42.00	81	30	44.40	42.20	78	35	
45.00 45.00	41.40 41.20	82 82	18 18	44.40	42.00 41.40	4) 79	3n 26	
45.00	41.00	69	19	44.40	41.20	79	26	
45.00	40.40	71	55	44.40	41.00	79	26	
45.00	40.20 40.00	71 69	22 19	44.40	40.40 40.20	68 68	25 25	
45.00	39.40	66	17	44.40	40.00	49	19	
45.00	39.20 39.00	66 66		44.40	39.40 -	69 69	19	
44.40	57.00	261	44	44.40	39.00	69	19 19	
44.40	76.40	561	44	44.20	57.00	239	40	
44.40 44.40	56.70	261 261	44	44.20	56.40 56.20	239 239	40	
44.40	55.40	261	44	44.20	56.00	239	40	
44.40	55.20	248	44	44.20	55.40	534	40	
44.40	55.00 54.40	248	44	44.20	55.20 55.00	234	40	
44.40	54.20	239	45	44.20	54.40	239	40	
44.40	54.00	231	53	44.27	54.20	559	39	
44.40	53.40 53.20	230 230	53	44.20	54.00	219 220	39	
44.40	53.00	227	53	44.20	53.20	221	23	
44.40	52.40	227	53	44.20	53.00	21A	23	
44.40 44.40	52.20 52.00	218	53	44.20	52.40 52.20	<u>509</u>	23	
44.40	51.40	155	53	44.20	52.00	504	23	
44.40	51.20 51.00	209	53	44.20	51.40	209 209	53	
44.40	50.40	198	53	44.20	51.20	500	53	
44.40	50.20	198	53	44.20	50.40	198	23	
44.40	50.00	198	53 53	44.20	50.00	198 93	23 #	
44.40	49.47	190	- 13 ¥	44.20	49.50	109	13 #	
44.40	49.30	180	4 #	44.20	49.40	35	5 🖫	
44.40	49.20	228 199	3 31 *	44.20 44.20	49.20	354 231	, , ,	
44.40	49.00	187	94 *	44.20	49.10	194	30 ₩	
44.40	48.50	146	115#	44.20	49.00	145	90 *	
44.40	48.30	186	5A 14	44.20 44.20	48.50 48.40	141 175	111 # 46 #	<u></u>
44.40	48.20	46	11	44.20	48.30	72	23 *	
44.40	40.10 48.00	32 27	51	44,20	48.20	29	23 **	
44.40	47.50	28	26 28	44.20	48.00	29 27	25 ° 27 *	
44.40	47.40	31	30	44.20	47.50	53	54 #	
44.40	47.30	37	30	44.20	47.40	19	33 🗰	

LAT	LONG	DIR	SPD					
44.20	47.30	19	34 *	44.00	47.40	12	*	
44.20	47.20	23	27 *	44.00	47.30	13 12	26 * 26 <u>*</u>	
44.20	47.10	36	50 #	44.00	47.20	ii	34	
44.20	46.50	48 65	16 #	44.00	47.10	12	21 *	
44.20	46.40	92	15 # 14 #	44.00	47.00	20 34	18 * 15 *	
44.20	46.30	109	16 *	44.00	46.40	53	15 #	
44.20	46.20	100	17	44.00	46.30	63	17	_
44.20	46.10 46.00	88 88	23 * 29 *	44.00	45.20	60	22 *	
44.20	45.40	66	37 *	44.00	46.00	60 69	35 *	
44.20	45.20	69	32 +	44.00	45.40	69	42 *	
44.20	45.00	69	32 #	44.00	45.20	68	43 *	
44.20	44.40	70	42	44.00	45.00	77	56 *	
44.20	44.00	68	44	44.00	44.40	69 68	47	_
44.20	43.40	68	44	44.00	44.00			
44.20	43.20	68	44	44.00	43.40	69	47	
44.20	43.00	4) 78	44	44.00	43.20	78	47	
44.20	42.20	78	35	44.00	43.00	78 81	47	
44.20	42.00	41	30	44.00	42.20	81	44	
44.20	41.40	74	24	44.00	42.00	78	35	
44.20	41.00	79	26	44.00	41.40	81	30	
44.20	40.40	78	24	44.00	41.20	81 81	30	
44.20	40.20	7A	23	44.00	40.40	79	30	
44.20	40.00	×2	18	44.00	40.20	79	56	
44.20	39.40 39.20	42	IA	44.00	40.00	79	24	
44.20	39.00	32	18 18	44.00	39.40	77	21	
44.00	57.00	220	39	44.00	39.00	77	21	_
44.00	56.40	220	39	43.40	57.00	220	39	
44.00	56.20	550	30	43.40	56.40	220	39	
44.00	56.00 55.40	550 550	39 39	43.40 43.40	56.20 56.00	220	34	
44.00	54.20	210	40	43.40	55.40	550	39	
44.00	55.00	210	40	43.40	55.20	510	40	
44.00	54.40	510	40	43.40	55.00	510	40	
44.00	54.00	210	40	43.40	54.40	210	40	
44.00	53.40	510	32	43.40	54.00	500	40 39	
44.00	53.20	208	29	43.40	43.40	201	32	
44.00	53.00	210	23	43.40	53.20	201	32	
44.00	52.40 52.20	501 504	23 23	43.40	53.00	198	29	
44.00	52.00	501	- 23	43.40	52.40 52.20	198	29 27	
44.00	51.40	191	23	43.40	52.00	259	55	
44.00	51.20	192	53	43.40	E1.40	161	27	
44.00	51.00 50.40	191 349	23	43.40	51.20	34	19	
44.00	50.20	347	23 23	43.40	50.40	99	55	
44.00	50.00	176	10#	43,40	50.20	64		
44.00	49.50	167	11+	43,49	50.00	241	10	
44.00	49.40	131	7 *	43.40 43.40	49.50	325	15	
44.00	49.20	187		43.40	49.40	288		
44.00	49.10	195	23 48 *	43.40	49.20	199	51	
44.00	49.00	195	83*	43.40	49.10	199	4 26	
44.00	48.50 48.40	190	56#	43.40	49.00	202	60	
44.00	48.30	50	24 # 9 #	43.40 43.40	48.50 48.40	204 215	36 11 *	·
44.00	48.20	9	21.	43.40	48.30	344	 ii *	
44.00	48.10	10	55.	43.40	48.20	351	55 #	
44.00	48.00 47.50	13	24 *	43.40	48.10	351	27 #	
	~ , , , ,	1	69	43.40	48.00	350	28 🛊	

LAT	LONG	DIR	SPD					
43.40	47.50	353	89 #	43.20	48.00	3	22 *	
43.40	47.40	356	32	43.20	47.50	0	29 *	
43.40	47.30 47.20	1	33 *	43.20	47.40	1	35 #	
43.40	47.10	8 16	* حُرَحُ ٠	43.20	47.30 47.20	3	38 #	
43.40	47.00	20	23 *	43.20	47.10	8 17	3A # 36 #	
43.40	46.50	56	25 #	43.20	47.00	27	34	
43.40	- 46.40	42	22 *	43.20	46.50	32	36 #	
43.40 43.40	46.20 46.20	57 50	37 #	43.20	46.40	32	44 *	
43.40	46.10	- · 45	TAB T	43.20	46.30	47	65 *	
43.40	46.00	50	50 *	43.20	46.10	55	65 #	
43.40	45.40	65	43.	43.20	46.00	60	h3 #	
43.40	45.20	59	44 *	43.20	45.40	46	64 🚆	
43.40	45.00 44.40	62 88	61# 64	43.20	45.20	70	',4	
43.40	44.20	48	64	43.20 43.20	45.00	40 79 -	<mark>58</mark>	
43.40	44.00	69	59	43.20	44.20	79	66	
43.40	43.40	79	72	43.20	44.00	79	-1	
43.40	43.20	78	47	43.20	43.40	H0	56	
43.40	43.00	41 02	44	43.20	43.20	79	42	
43.40 43.40	42.40 42.20	90	46	43.20	43.00	79	49	
43.40	42.00	90	46	43.20 43.20	42.40 42.20	-11	44	
43.40	41.40	40	34	43.20	42.00	41 41	44	
43.40	41.20	→ 0	34	43.20	41.40	90	34	
43.40	41.00	4 0 ¯	14	43.20	41.20	90	34	
43.40	40.40	90	27	43.20	41.00	40	34	
43.40 43.40	40.20 40.00	96 ' ' '	27	43.20	40.40	30	27	
43.40	39.40	90	25	43.20	40.00	40	27	
43.41	39.20	9 (1	25	43.20	34.40	90	27 25	
43.40	39.00	. 42	5€	43.20	39.20	40		
43.20	57.00	190	40	43.20	39.00	40	24	
43.20 43.20	55.40 56.30	1 20.	46	43.00	~7.00	180	34	
43.20	56.20 56.00	190	40	43.00	56.40	180	39	
43.20	55.40	190	40	43.00 43.00	56.20 56.00	180 180	39	
43.20	55.20	190	40	43.00	55.40	180	3 9	
43.20	55.00	140	40	43.00	55.20	140	39	
43.20	54.40	140	40	43.00	55.00	140	39	
43.20	54.20 54.00	190	40	43.00	54.40	140	39	
43.20	53.40	140	37	43.00	54.00	140	39	
43.20	53.20	190	37	43.00	53.40	180 180		
43.20	53.00	1 + 0	34	43.00	53.20	169	37	
43.20	52.40	140	35	43.00	53.00	161	36	
43.20	52.20	188	30	43.00	52.40	169	37	
43.20	52.00 51.40	254 6	7 *	43.00	52.20	169	37	
43.20	51.20	343	-14-#	43.00	52.00 51.40	195 219	9#	
43.20	51.00	34	6 *	43.00	51.20	546	25 *	
43.70	50.40	86	A.*	43.00	51.00	304	74 #	
43.20	50.20	190	7 🚜 👢	43.00	50.40	266	29 🚆	
43.20	50.00	159	14 #	43.00	50.20	565	32 #	
43.20	49.50	195 214	7 * 27 *	43.00 43.00	50.00 49.50	241	4 0	
43.20	49.30	213	51 *	43.00	₹6°₹U #A•2U	227 221	53 * 59 *	_
43.20	49.20	204	84 #	43.00	49.30	215	54 1	
43.20	49.10	202	60 🚜	43.00	49.20	210	37 *	
43.20	49.00	199	33 #	43.00	49.1n	501	18 #	
43.20	49.50 48.40	203		43.00	49.00	143		
43.20	48.30	30	16 *	43.00 43.00	48.40	43	12 *	
43.20	4H.20		17.*	43.00	48.30	50	- 15 *	
43.20	48.10	13	ÎA #	43.00	48.20	16	15.8	

LAT	LONG	DIR	SPD				
43.00	4R.10	20	17 *	42.40	48.20	29	25 *
43.00	48.00	19	24 *	42.40	48.10	28	27
43.00	47.50	[]	33 🚜	42.40	48.00	27	36
43.00	47.40	17	40	42.40	47.50	25	42
43.00	47.3n	16	45 #	42.40	47.40	25	42 *
43.00	47.20	15	4H *	42.40	47.30	55	40 *
43.00	47.1n	17	49 #	42.40	47.20	15	45 *
43.00	47.00	25	55 *	42.40	47.10	13	
43.00	46.50	31	61 *	42.40	47.00	14	36 *
43.00	46.40	32	79.*	42.40	46.50	<u>19</u>	
43.00	46.30	35	H7 *	42.40	46.40	30	76.*
43.00	46.20	73	63*	42.40	46.20	28	77 *
43.00	46.10		64 *	42.40	46.10	40	72 *
43.00	45.00 45.40	160	33 *	42.40	45.00	" ' ys	
43.00	45.20	79	52	42.40	45.40	69	52 *
43.00	45.00	40	54	42.40	45.20	79	42
43.00 43.00	44.40	H()	54	42.40	45.00	79	52
43.00	44.20	30		42.40	44.40	90	41
43.00	44.00	40	55	42.40	44.20	90	48
43.00	43.40	90	4.9	42.40	44.00	90	49
43.00	43.20	40	46	42.40	43.40	40	44
43.00	43.00	94	44	42.40	43.20	99	42
43.00	42.40	100	40	47.40	43.00	99	42
43.00	42.20	100	40	42.40	42.40	94	30
43.00	42.00	100	40	42.40	42.20	9A	30
43.00	41.40	101	35	42.40	42.00	3 _H	30.
43.00	41.20	101	35	42.40	41.40	108	36
43.00	41.00	100	37	42.40	41.20	1.0 W	36
43.00	40.40	100	41	42.40	41.00	108	36
43.00	40.20	100	40	42.40	40.40	100	42
43.00	40.00	40	30	42.40	40.20	109	42
43.07	39.40	٩n	23	42.40	40.00	103	47
43.00	34.20	40	23	42.40	39.41	111	25
43.00	39.00	90	73	42.40	30.50	111	25
42.40	57.00	149	40	42.40	39.00	111	25
42.40	56.47	144	40	42.20	-7.00	120	40
42.40	56.20	159	39	42.20	56.40	120	40
42.40	56.00	159	39	42.20	46.20	130	47
42.40	55.40	159	34	42.20	56.00	130	4?
42.45	55.20	169	4.0	42.20	55.40	141	44
42.40	55.00	170	42	42.20	55.20	141	44
42.40	54.40	170		42.20	55.00	149	45
42.49	54.20	170	42 42	42.20	54.41 54.21	149	45
47.40	54.00	170	42	42.20	54.00	149	45
42.40	53.40	160 150	42	42.20 42.20	53.40	139	47
47.40	53.20 53.00	139	42	42.20	53.20	134	42
42.40	52.40	130	 45 *	42.20	53.00	130	42
42.40	52.20	119	42 *	42.29	52.40	120	45
42.40	52.00	196	17*	42.20	52.20	110	47
42.40	51.40	144	11 *	42.20	52.00	63	29,4
42.40	51.20	256	4 4	42.21	51.40	124	·····································
42.40	51.00	253	21 🖁	42.20	51.20	130	76
42.40	50.40	757		42.20	51.00	125	TA
42.40	50.20	248	36 *	42.20	50.40	192	i>*
42.40	50.00	235	47 *	42.20	50.20	185	
42.40	49.50	234	40 *	42.20	50.00	128	13*
47.40	49.40	247	25 %	42.20	49.51	93	19*
42.40	44.30	278	12 *	42.20	49.40	42	24 *
42.40	44.20	320	3 #	42.20	49.30	77	25 * 24 * 22 *
42.40	49.10	46	4 👱	42.20	49.20	74	24 🖁
2.40	49.00	79	7 <u>*</u>	42.20	49.11	70	72.7
47.40	48.50	59	ý *	42.20	44.00	66	22 🕇
42.40	48.40	40	13*	42.20	4R.50	63	24 *
	48.30	11] A #	42.20	48.40	59	27 *

LAT	LONG	DIR	SPD					
42.20	48.30	52	30 *	42.00	48.40	66	21 #	
42.20	48.20	45	31 🔭	42.00	4A.30	58	15 #	
42.20	48.10	40	33	42.00	48.20	36	134	
42.20	4R.00	28	31 *	42.00	48.10	358	12	
42.20 42.20	47.50 47.40	12 359	30 *	42.00 42.00	48.00	50	7 A *	
42.20	47.30	- 0	34 #	42.00	47.50	<u>25</u>	25 #	
42.20	47.20	5	45 #	42.00	47.30	1	46 #	
42.20	47.10	6	65 x	42.00	47.20	3	60 #	
42.20	47.00	3	94	42.00	47.10	7	70 #	
42.20	46.40		111 ** 88.*	42.00 42.00	47.00	2	92 *	
42.20	46.30	13	54 *	42.00	46.40	356	101*	
42.20	46.20	14	71 *	42.00	46.30	ž	93*	
42.20	46.17	7	79*	42.00	46.20	9	<u>~1#</u>	
42.20 42.20	45.40	······	62*	42.00	46.10	324	17*	
42.20	45.20	78	52 47	42.00 42.00	46.00	304	3H #	
42.20	45.00	78	47	42.00	45.40	70 70	42	
42.20	44.40	40	44	42.00	45.00	70	42	
42.20	44.20	40	41	42.00	44.40	79	40	
42.20	44.00	90	41	42.00	44.20	90	39	
42.20	43.40 43.20	90 100	37 37	42.00 42.00	44.00	90	37	
42.20	43.00	101	35	42.00	43.40	90	37	
42.20	42.40	98	30	42.00	43.00	40	34	
42.20	42.20	9-	30	42.00	42.40	90	3n	
42.20	42.00	94	30	42.00	42.20	20	30	
42.20	41.40 41.20	108	35	42.00	42.00	92	30	
42.20	41.00	108	36	42.00 42.00	41.40	- 9 4	30	
42.20	40.40	109	42	42.00	41.00	104	30 29	
42.20	40.20	100	42	42.00	40.40	102		
42.20	40.00	104	42	42.00	40.20	108	29	
42.20 42.20	39.44	111	75	42.00	40.00	10=	59	
42.20	39.20	111	25 24	42.00	39.40	102	21	
42.00	57.00	100	40	42.00 42.00	34.20	105	21 21	
42.00	56.46	100	40	41.40	57.00	30	79	
42.00	56.20	110	39	41.40	56.40	40	39	
42.00	56.00	109	47	41.40	56.20	90	41	
42.00	55.40 55.20	119	42	41.40	56.00	94	44	
42.00	55.00	130	39	41.40	55.47 55.20	9A	44	
42.00	54.40	159	4A	41.40	55.00	98	44	
42.00	54.20	129	48	41.40	54.40	110	47	
42.00	54.00	129	4A	41.40	54.20	110	<u> </u>	
42.00	53.40 53.20	128	44	41.40	54.00	109	49	
42.00	53.00	150 151	44	41.40	53.40	110	47	
42.00	52.40	119	47	41.40	53.20 53.00	110	47	
42.00	52.20	110	47	41.40	52.40	100	52	
42.00	52.00	70	34"#	41.40	52.20	100	44	—- -
42.00	51.40	137	29 *	41.40	52.00	100	72	
42.00 42.00	51.20 51.00	174 133	45 # 47 #	41.40	51.40	358	23*	
42.00	50.40	114		41.40 41.40	51.20	108	35 *	
42.00	50.20	44	37 *	41.40	50.40	36	58#	
42.00	50.00	aη	45 *	41.40	50.20	94	77	
42.00	49.50	72	51 *	41.40	50.00	77	91 <u>.</u> .	
42.00	49.40	12	52 % 49 #	41.40	49.50	79	7A 72 #	
42.00	49.21	94	43 #	41.40 41.40	49.40	100		
42.00	49.10	101	34	41.40	49.20	102	69#	
42.00	49.00	35	39 °	41.40	49.10	100	6A.	
42.00	44.50	74	27 *	41.40	49.00	101	68 #	

LAT	LONG	DIR	SPD					
41.40	48.50	103	67*	41.20	49.00	112	20.4	
41.40	48.40	105	61 *	41.20	48.50	113 124	3A *	
41.40	4H.30	100	54	41.20	48.40	132	29 *	
41.40	48.20 48.10	94 25	45 * 55 *	41.20	48.30	124	29 *	
41.40	48.00	61	33*	41.20	48.20 48.10	100 106	3A * 52 *	
41.40	47.50	44	36#	41.20	48.00	109		
41.40	47.40	44	42*	41.20	47.50	115	49 *	
41.40	47,30	46 32	57 74	41.20	47.40	26	41 *	
41.40	47.10	23	97*	41.20	47.20	<u>6</u> 34	92 *	
41.40	47.00	18	A3,*	41.20	47.10	83	44.4	
41.40	46.50	14 60	54*	41.20	47.00	49	47	
41.40	46.40 46.30		47	41.20 41.20	46.50	69	47	
41.47	46.20	รห์	49	41.20	45.40 46.30	71 64	44	
41.45	46.10	79-	45	41.20	46.20	50	42	
41.40	46.00	60	42	41.20	46.10	59	46	_
41.40	45.40 45.20	60 60	37 37	41.20 41.20	44.00	50	37	
41.40	45.00	58	35	41.20	45.40	61	35	
41.47	44.40	71	36	41.20	45.00	5)	29	
41.40	44.20	78	35	41.20	44.40	44	31	
41.40	44.00		34	41.20	44.20	50	33	
41.40	43.20	101	35	41.20	44.00	48 40	32 32	
41.40	43. 10	1 v 1	र प	41.20	43.20	101	35	
41.40	42.40	90)	30	41.20	43.00	109	54	
41.40	42.00	54 26	30	41.20	42.40	109	40	
41.40	41.40		25	41.20	42.20	100	49	
41.40	41.20	114	23	41.20	41.40	111	25	
41.40	41.00	113	23	41.20	41.27	111	25	
41.40 -41.40	4በ.4በ 4 ቫ. 2ቫ -	131	24	41.20	41.00	119	23	
41.40	40.00	119	18	41.20	40.20	119	23 24	
41.40	39.40	119	13	41.20	40.00	131	24	
41.40	34.20	119	14	41.20	39.40	119	18	
41.40	57.00	40	39	41.20	39.20	119	IA	
41.20	56.40	- 90	35	41.20	39.00	119 79	1 A	
41.20	56.20	40	39	41.00	56.40	79	40	
41.20	56.00	40	41	41.00	E6.20	80	42	
41.20 41.20	55.40 55.20		- 44	41.00	54.00	31	44	
41.20	55.00	40	48	41.00	55.20	9ŋ 90	4A 4A	
41.20	54.40	· · · • • • · · · · · · · · · · · · · ·	4A	41.00	55.00	40		
41.20	54.20	90	48	41.00	54.40	90	55	
41.20	53.40	40	4A 46	41.00 41.00	54.20	96	54	
05.14	53.20	90	48	41.00	54.00 53.47	40		
41.20	53.00	90	51	41.00	53.20	90	ร์ร์	
41.70	57.40	. 4ŋ	57	41.00	53.00	90	45	
41.20	52.20 52.00	- 30	55 55	41.00	52.40	90	55	
41.20	51.40	40	55 55	41.00	52.20	90	58	-
41.20	51.20	90		41.00	51.47	96	<u> </u>	
41.20 41.20	51.00 50.40	110	65 #	41.00	51.20	90	58	
41.20	50.20	102	47 # 47 #	41.00	51.00 50.40	90	55	
41.70	50.00	76	68	41.00	50.20	40	53 82 *	
41.20	44.50	94	68 * 62 * 51 **	41.00	50.00	57	61 *	
41.20 41.20	49.4 <i>0</i> 44.30	195	5] **	41.00	49.50	127	59 #	
41.20	49.24	103	45 *	41.00	49.40	147	61 *	
41.20	49.10	106	40#	41.00	49.20	159	30 *	
							*	

LAT	LONG	DIR	SPD				
41.00	49.10	171	28 *	40.40	49.20	90	51
41.00	49.00	145	51 *	40.40	49.10	90	51
41.00	48.50	90	51	40.40	49.00	90	48
41.00	48.4P	۸ù	51	40.40	48.50	90	48
41.00	48.30	40	51	40.40	48.40	90	48
41.00	48.20	90	51	40.40	48.30	90	46
41.00	48.10	44 78	49	40.40	48.20	90	44
41.00	48.00	— 78 —		40.40	48.00	90	
41.00	47.40	81	44	40.40 40.40	47.50	90 90	41
41.00	47.30		44	40.40	47.40	90	<u>41</u>
41.00	47.20	หง	42	40.40	47.30	90	39
41.00	47.10	40	42	40.40	47.20	90	37
41.00	47.00	80	42	40.40	47.10	82	37
41.00	46.50	79	40	40.40	47.00	78	35
41.00	46.40	79	37	40.40	46.50	78	
41.00	46.30	75	3A	40.40	46.40	78	35
41.00	46.20 46.10	71 53	36 36	40.40	46.30	74	33
41.00	46.00	58	35 35	40.40	46.20	67 53	30
41.00	45.40		32	40.40	46.00		31
41.00	45.20	61	29	40.40	45.40	61	29
41.00	-45.00		59	40.40	45.20	48	74
41.00	44.40	61	20	40.40	45.00	29	13
41.00	44.20	3~	29	40.40	44.40	8	16
41.00	44.70	91	30	40.40	44.20	8	16
41.00	43.40	94	30	40.40	44.00	18	14
41.00	43.20	112	31	40.40	43.40	34	
41.00	43.00 42.40	102	3n 21	40.40	43.20	50	23
41.00	42.20	20	50	40.40	43.00	77	
41.00	42.00	40	50	40.40	42.40	40	21
41.00	41.40	97	18	40.40	47.00	90	7n
41.00	41.20	97	18	40.40	41.40	J0	11
41.00	41.00	J15 -	14	40.40	41.20	90	11
41.00	40.40	119	13	40.40	41.00	101	11
4. 700	40.20	119	1 ค	40.40	40.40	111	15
41.00	40.00	119	18	40.40	40.20	12-	11
41.00	39.20	116	15	40.40	40.00	156	11
41.00	39.00	116 116	15 15	-40.40 -40.40	39.40 	126	11
40.40	57.00	51	44	40.40	33.00	111	12
40.40	56.40	78	47	40.20	57.00	79	12
40.40	56.20	79	49	40.20	56.40	79	49
40.40	56.00	79	52	-40.2n	56.21	··· 79 - ·	40
40.40	55.40	80	54	40.20	56.00	40	54
40.40	55.20	30	54	40.20	55.40	Bl	54
40.40	55.00	40	5R	40.20	55.20	H0	5a
40.40	54.40	40	62	40.20	55.00	40	58
40.40	54.20 EX.74	90	65	40.20	54.40	90	
40.40	54.01 53.40	40	65°	40.20	54.20	•0	ችና
-45.45	53.20	90	65	40.20	53.40	30	65
40.40	53.00	40	65	40.20	53.20	90	65
40.40	52.40	90	65	40.20	53.00	90	65
40.40	52.20	40	65	40.20	52.40	90	65
40.40	52.00	40	65	40.20	52.20	90	65
40.40	51.40	90	62	40.20	52.00	40	65
40.40	51.20	90 -	62	40.20	51.40	90	95
40.40	51.00	90 90	62	40.20	51.20	90	65
40.40	50.40 50.20	40	65 65	40.20	51.00	90 90	62
40.40	50.00		55	40.20	50.40 50.20	90	65
40.40	49.50	40	ร์ร์	40.20	50.20	90	60
40.40	49.40	40	53	40.20	49.50	90	5A
40.40	49.30	40	53	40.20	49.40	90	55

LAT	LONG	DIR	SPD					
40.20	49.30	90	53	40.00	49.40	90	48	
40.20	44.20	40	51	40.00	49.30	90	4.8	
40.20	-44.1n	90	51	40.00	49.20	90	48	
40.20	49.00	40	4.P	40.00	49.10	90	48	
40.20	48.50	90	46	40.00	49.00	90	46	
40.20	49.40	40	44	40.00	48.40	90	44	
40.20	48.20	90	41	40.00	48.30	90	41	
40.20	48.10	90	46	40.00	4H.20	90	41	
40.20	4 H . 00	90	44	40.00	48.10	90	34	
40.20	47.50	- 40	41	40.00	4A.00	90	34	
40.20	47.40	90	74	40.00	47.50	90	32	
40.20	47.30	90	37 37	40.00	47.40	90	30	
40.20 40.20	47.20 47.10	100 105	33	40.00 40.00	47.30	98	<u>3</u> 0	
40.20	47.00	112	30	40.00	47.10	107	31	
40.20	46.51	112	3:1	40.00	47.00	112	3.0	
40.20	440	108	29	40.00	46.50	112	30	
40.20	45.30	114	24	40.00	46.40	119	27	
40.20	46.20	120	27	40.00	46.30	116	54	
40.20 40.20	46.IO 45.OO	120 120	27 == 27	40.00 40.00	46.27 46.10	119	23 23	
40.20	45.40	131	24	40.00	46.00	$-\frac{119}{119}$	23	
40.20	45.20	150	23	40.00	45.40	131	24	
40.20	45.00	154	23	40.00	45.20	150	23	
40.20	44.40	347	21	40.00	45.00	167	21	
40.70	44.20	n	21	40.00	44.40	351	16	
40.20	44.00	4 -	21	40.00	44.20		16	
40.20 40.20	43.40	49 -0	21 23	40.00 40.00	44.00	11	16 23	
40.20	43.20		25	40.00	43.20	16	 22	
40.20	42.40	78	23	40.00	43.00	24	23	
40.20	42.20	3.0	21	40.00	47.40	Zŋ	71	
40.20	42.00	-۲	20	40.00	42.20	49	21	
40.20	41.40	30	11	40.00	42.0h	60	53	
40.20	41.20	-10	11	40.00	41.40	H	12	
40.20	41.00	191 191	11	40.00 40.00	41.20	78	11	
40.20	40.20	111	12	40.00	40.40			
40.20	40.00	iii	12	40.00	40.20	101	ii	
40.20	39.40	101	11	40.00	40.00	101	- 11	
40.20	39.20	101	11	40.00	39.40	101	11	
40.20	39.00	101	11	40.00	34.20	101	71	
40.00 40.00	57.00 54.40	70 70	54 54	40.00	34.00	101	· · · · · · · · · ·	
40.00	56.40 56.20	40	54 54	0.00	0.00	444	',	
40.00	56.00	80	58					•
40.00	55.40	40	44					
40.00	55.20	80	54					
40.00	55.00	<u>40</u>	5.9					
40.00 40.00	54.40 54.20	79 79	63 63					
40.00	54.00	90	65					
40.00	53.40	40	65					
47.00	53.20	40	65			— — — — — — — — — — — — — — — — — —		
40.00	53.00	→ ()	65					
40.00	52.40	30	65					
40.00	52.20 53.00	→ 0	65 65					
40.00 40.00	52.00 51.40	40	42 42					
40.00	51.20	70	52					
40.00	61.00	40	62					
40.00	50.40	9.0	42 °					
40.00	50.20	÷0	. 52					
40.0n	50.00	40 40	· 55					
40.00	49.50	→0	53					

DATE FILMES